Fig.77A

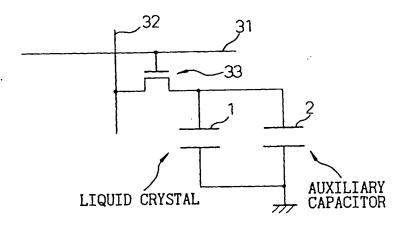


Fig.77B

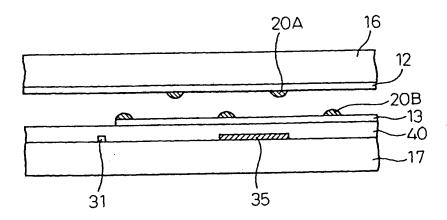


Fig.78A

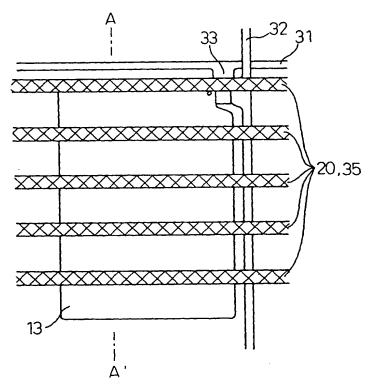
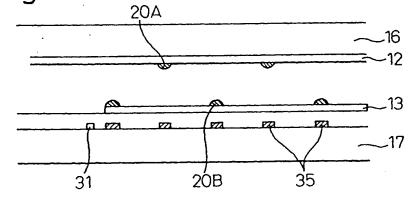
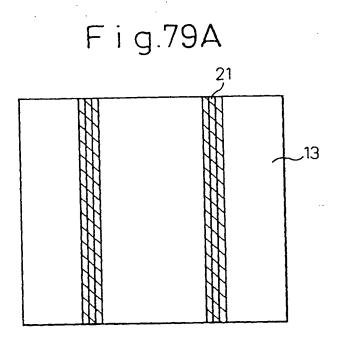
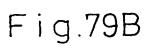
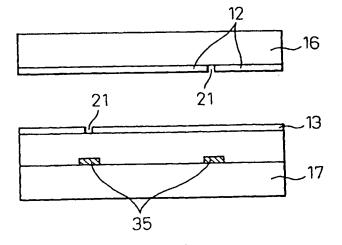


Fig.78B









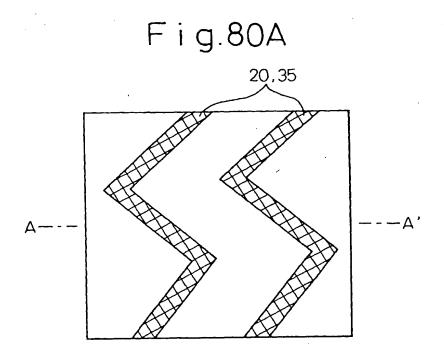
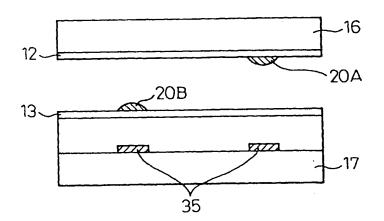
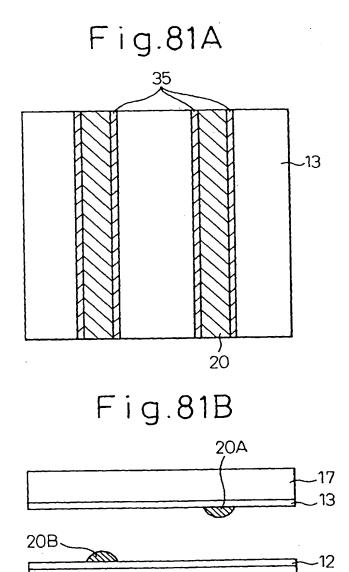


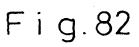
Fig.80B

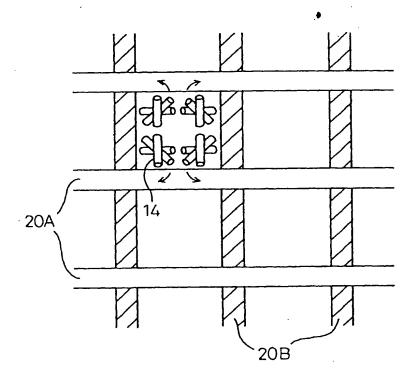




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\_16





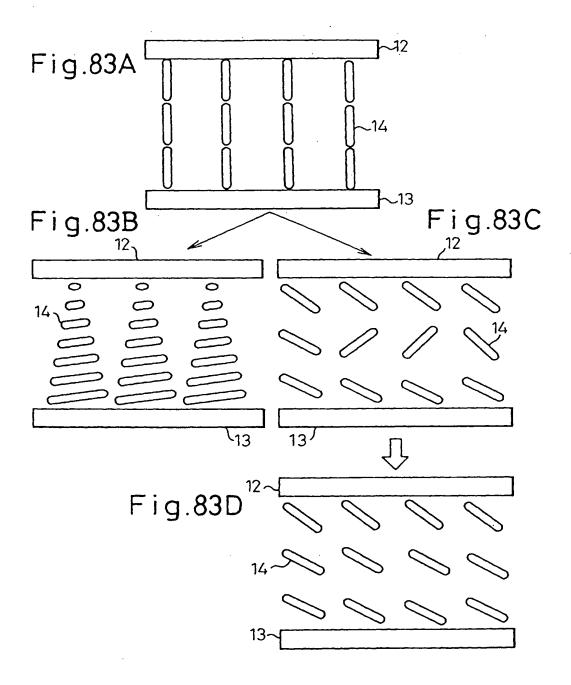
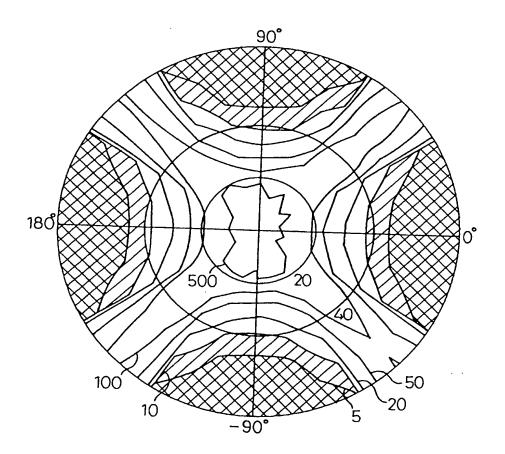
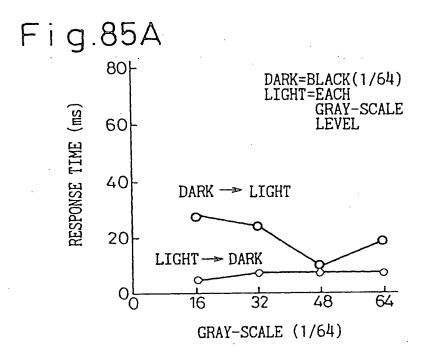
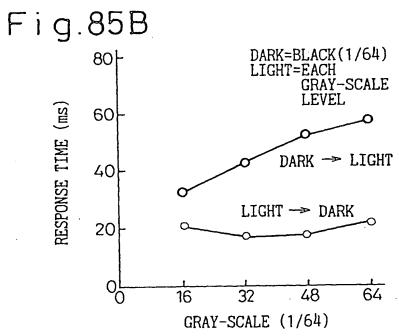
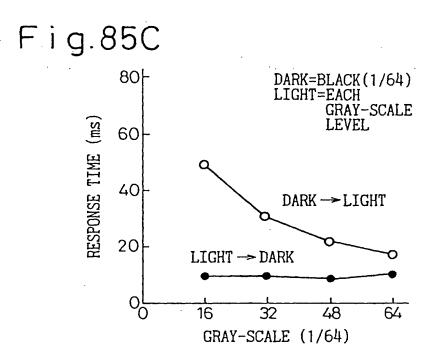


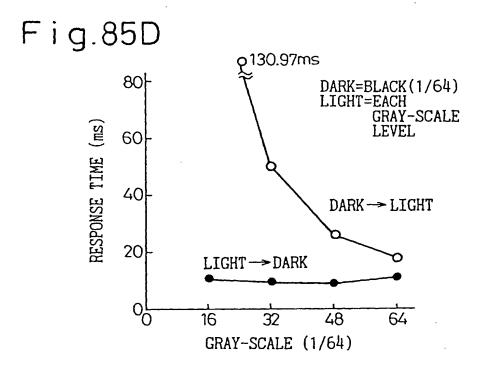
Fig.84











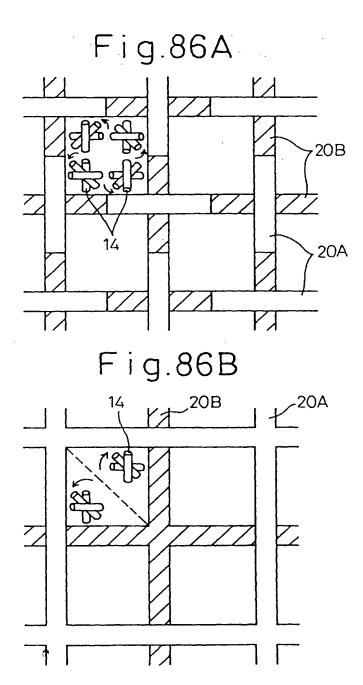
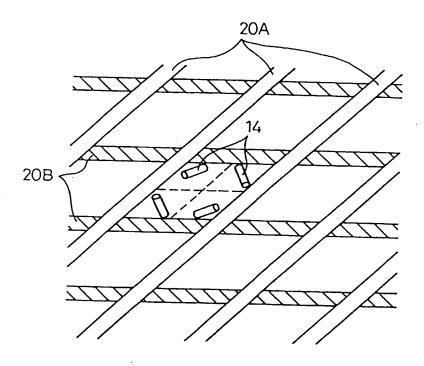
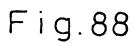


Fig.87





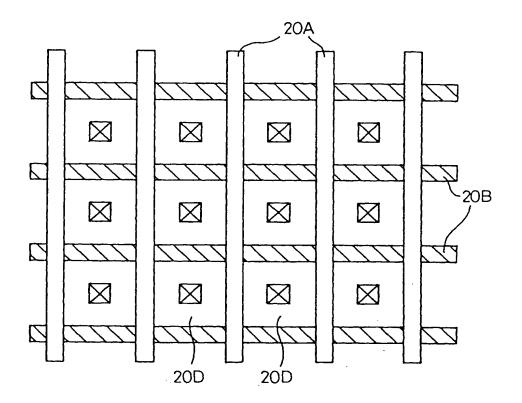


Fig.89

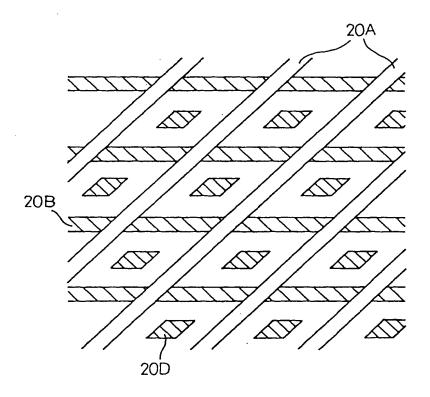


Fig.90A

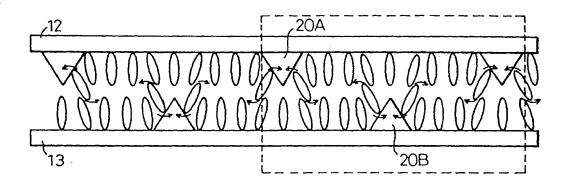


Fig.90B

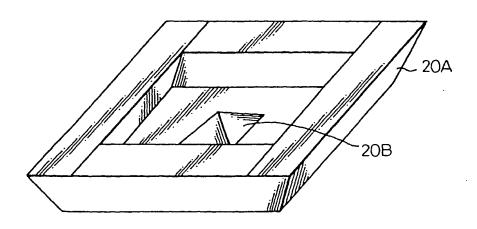


Fig.91

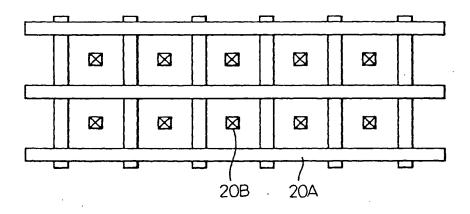


Fig.92A

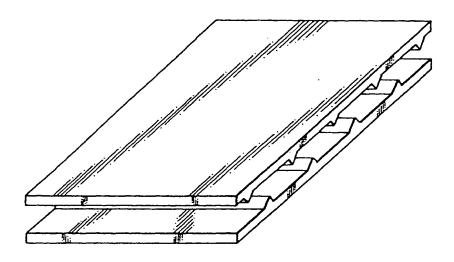


Fig.92B

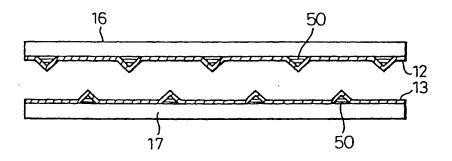


Fig.93

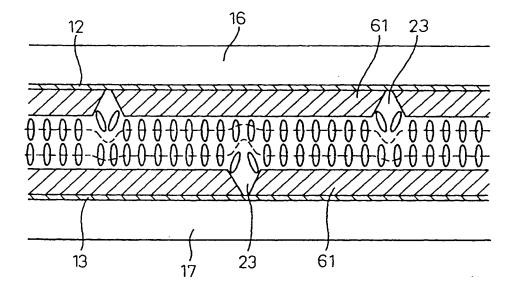


Fig.88

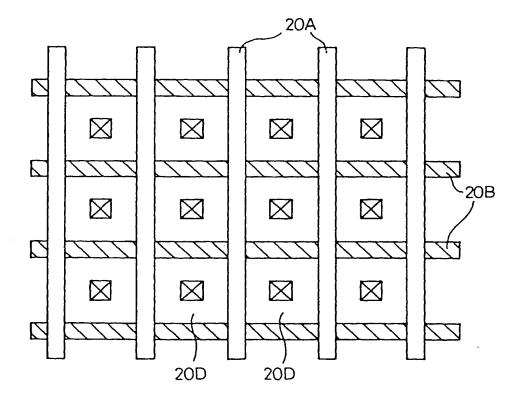


Fig.94

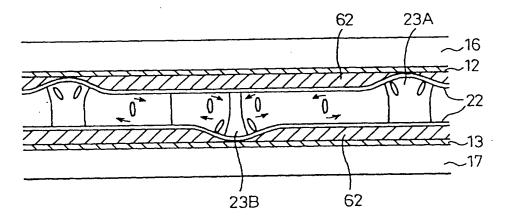
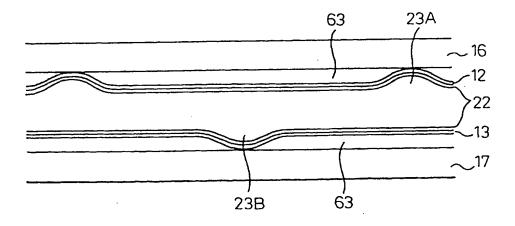
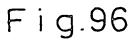


Fig.95





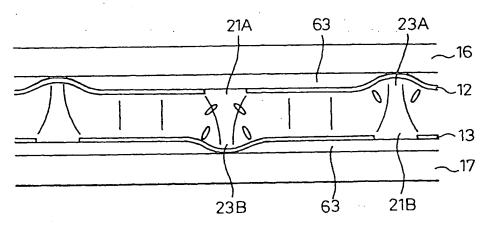


Fig.97

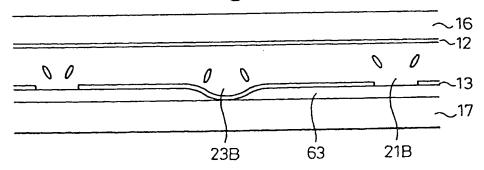


Fig.98

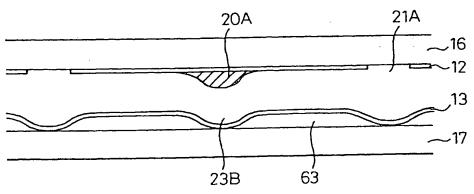


Fig.99A

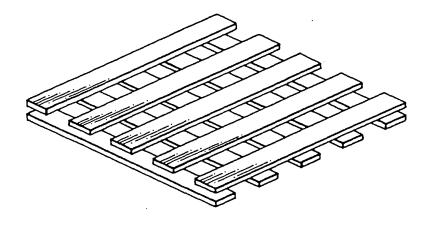
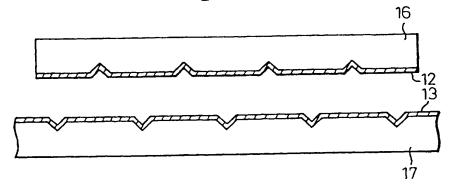


Fig.99B



## Fig.100A

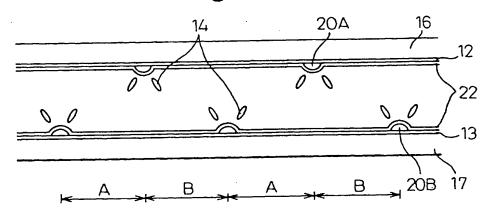


Fig.100B

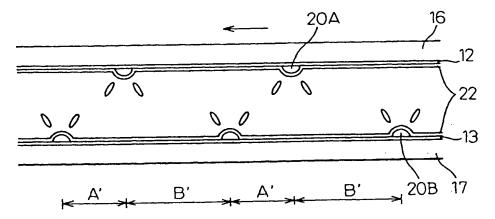


Fig.101A

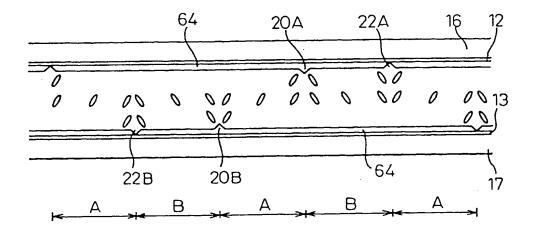


Fig.101B

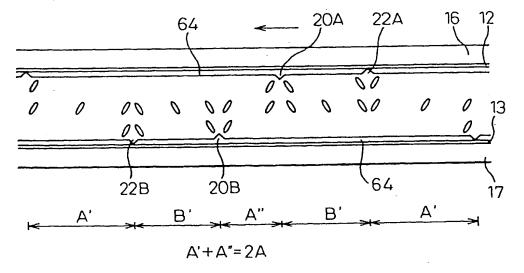


Fig.102

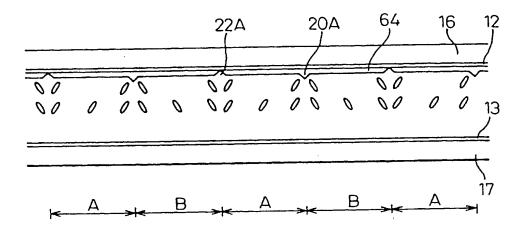


Fig.103A

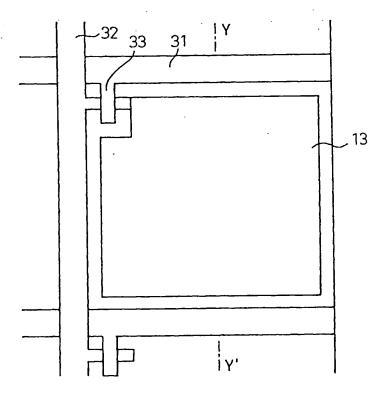


Fig. 103B

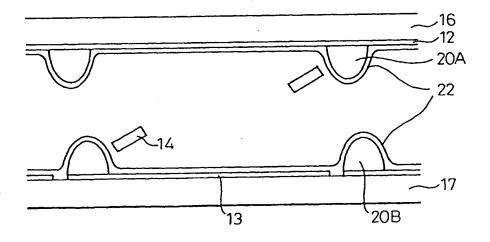
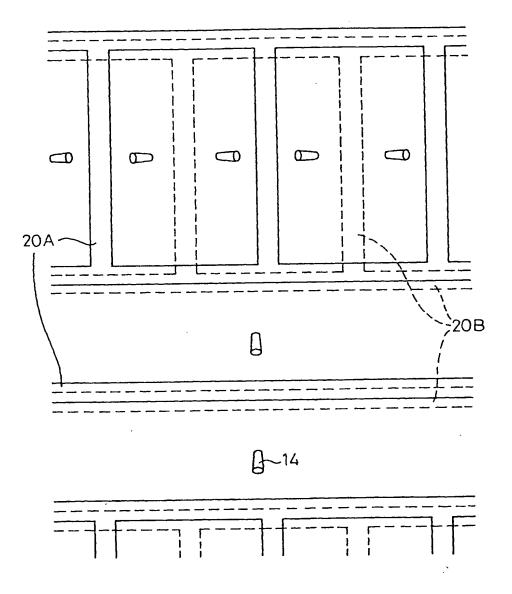
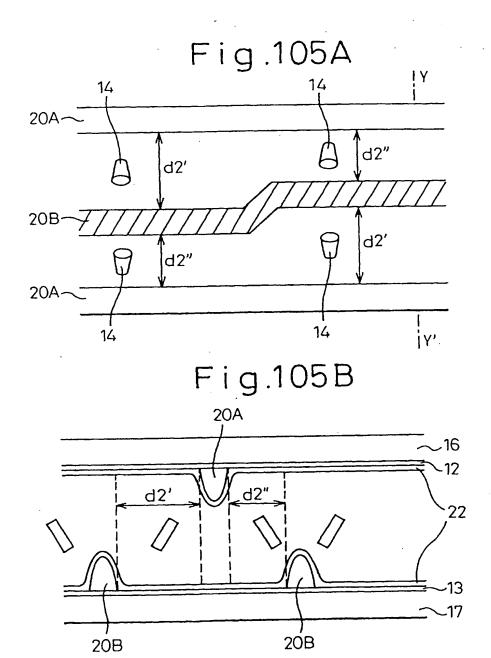


Fig.104





## Fig.106

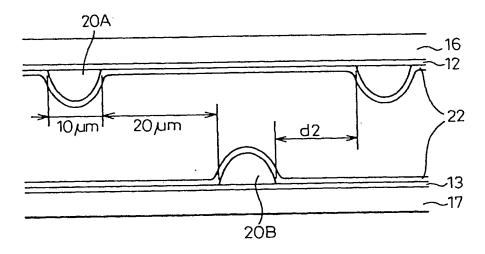
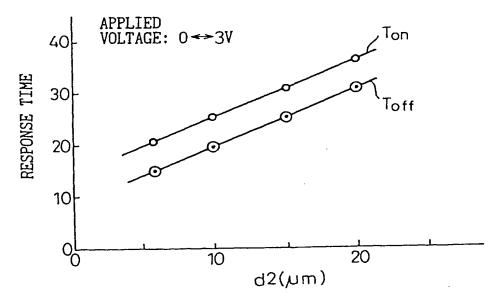
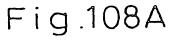


Fig.107





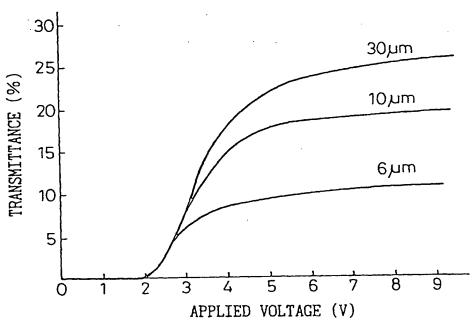
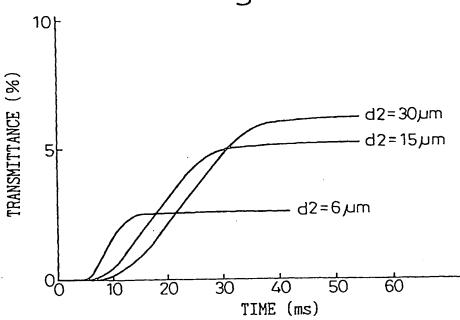
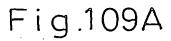


Fig.108B





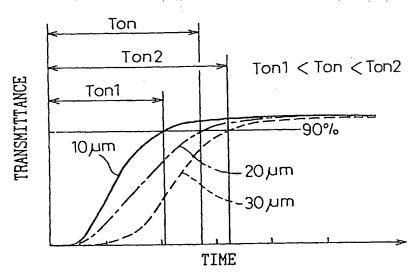


Fig.109B

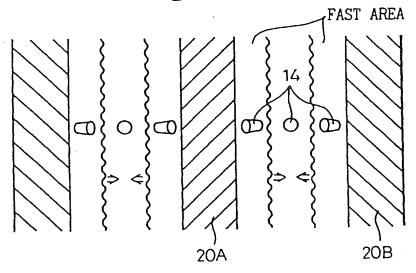


Fig.110

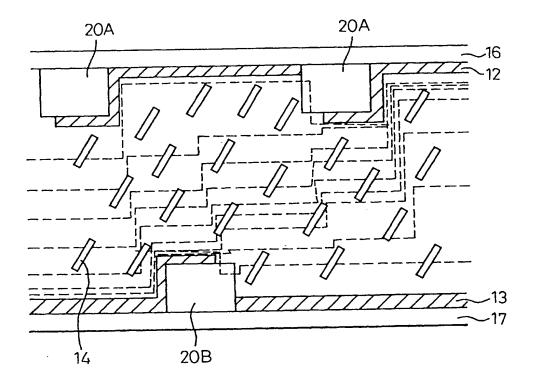


Fig.111

CONTRAST	RATIO
	100.000 50.000 20.000 10.000 5.000

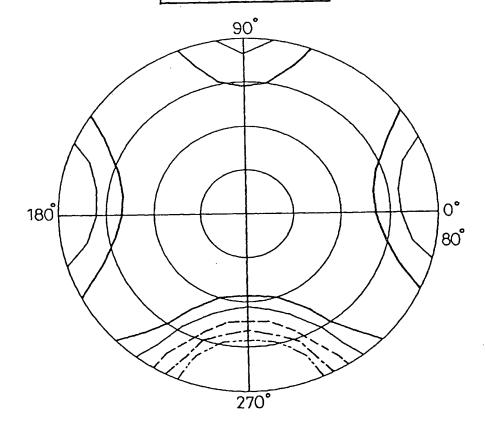


Fig.112

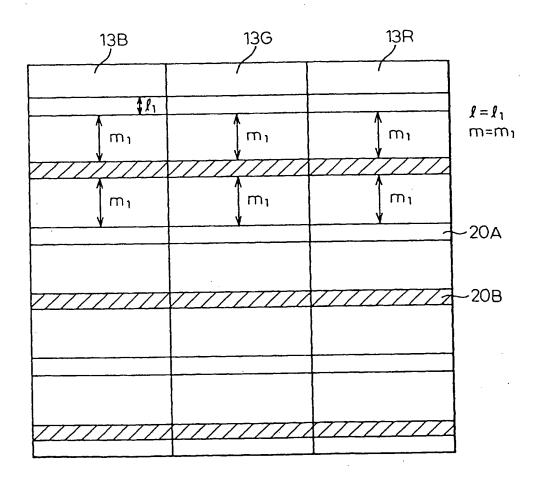


Fig.113

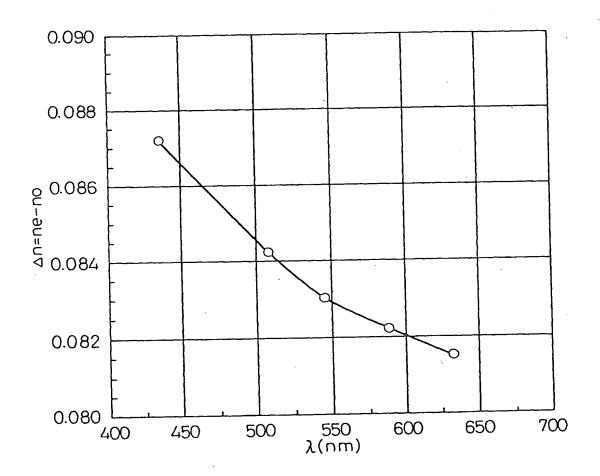


Fig.114

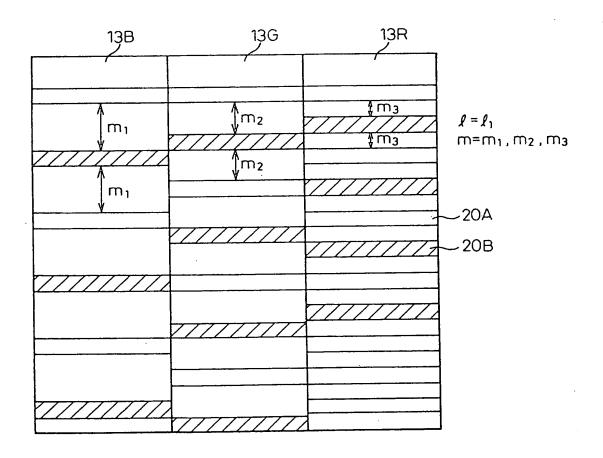


Fig.115

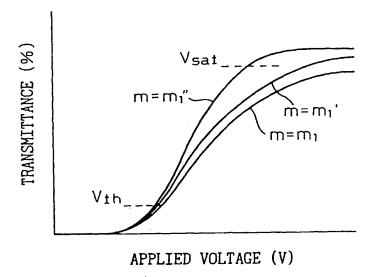


Fig.116

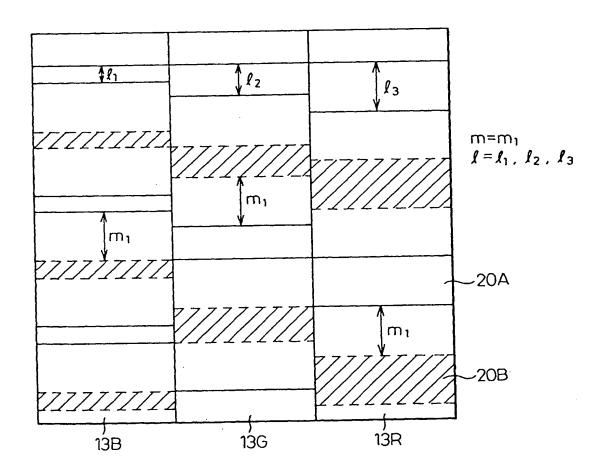


Fig.117

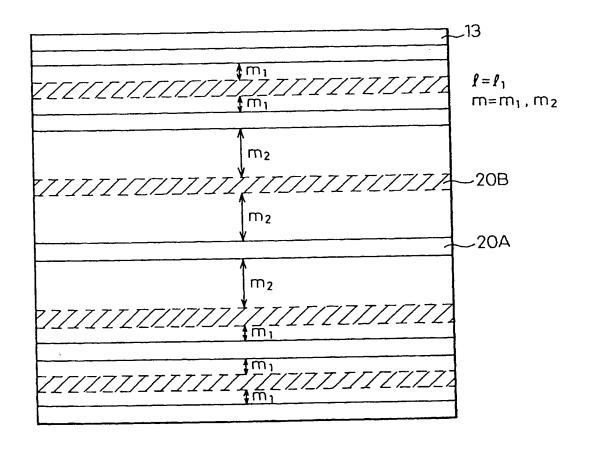
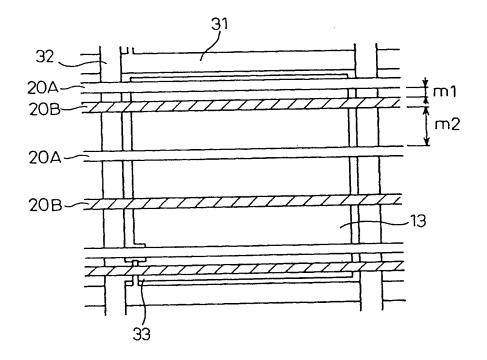
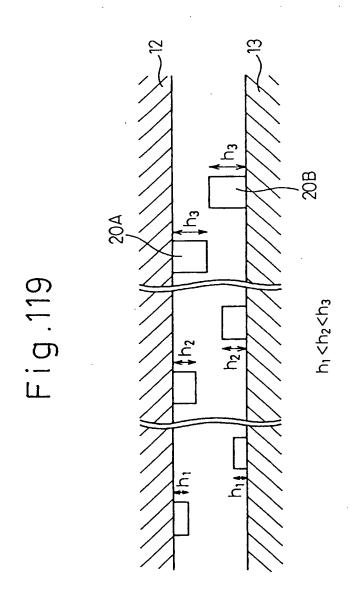
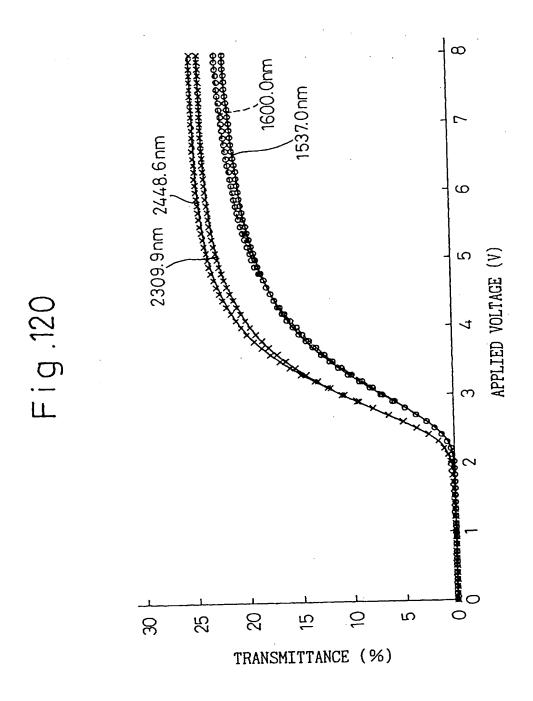
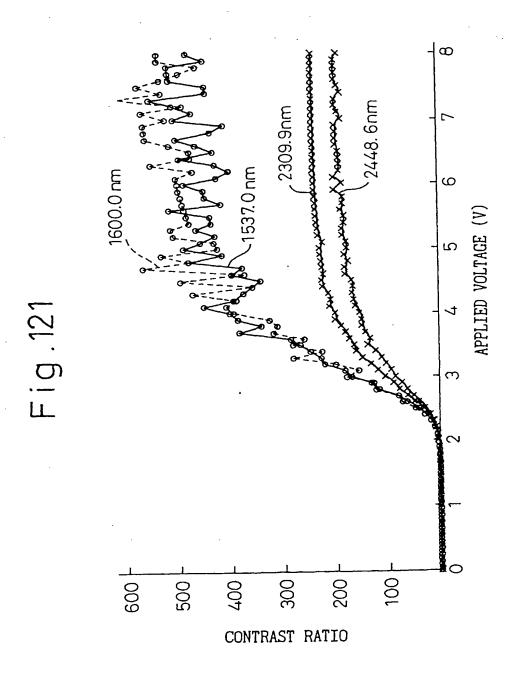


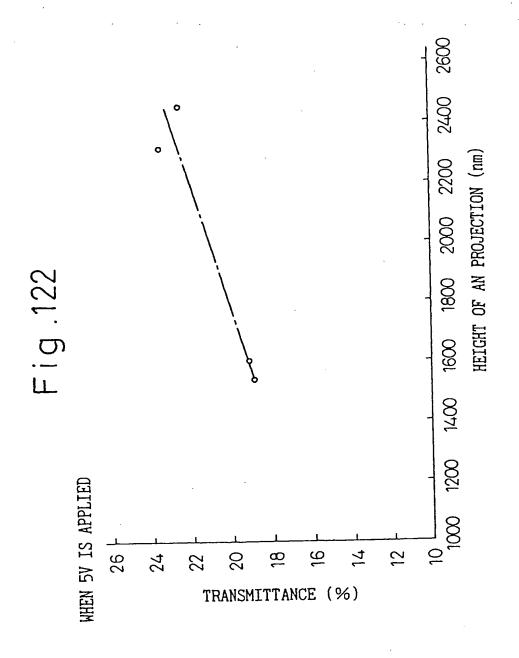
Fig.118

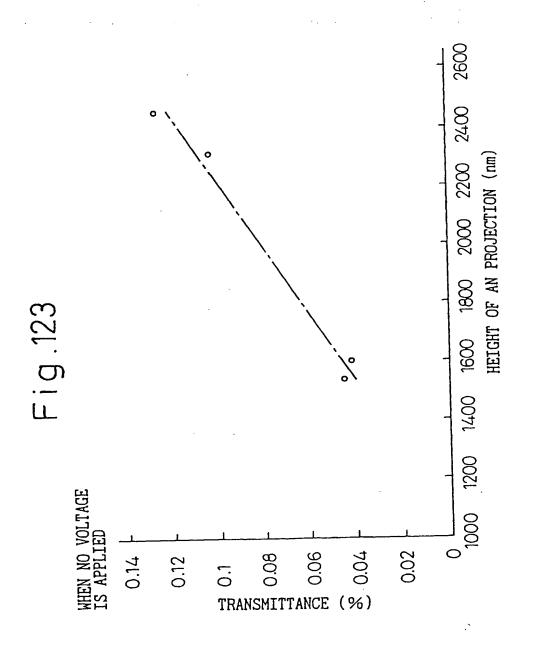


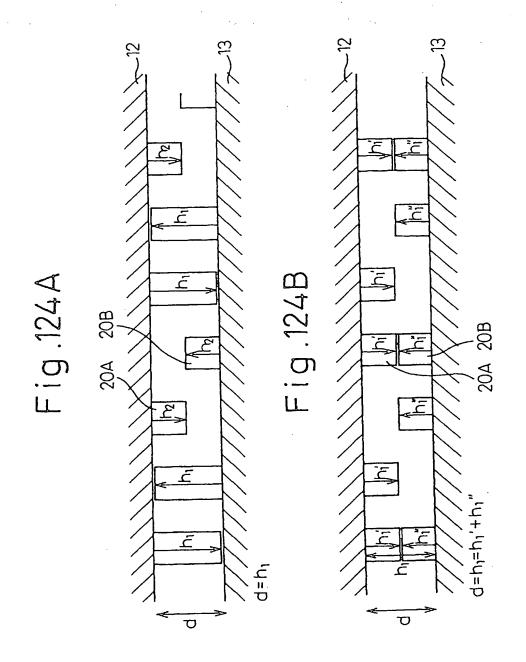












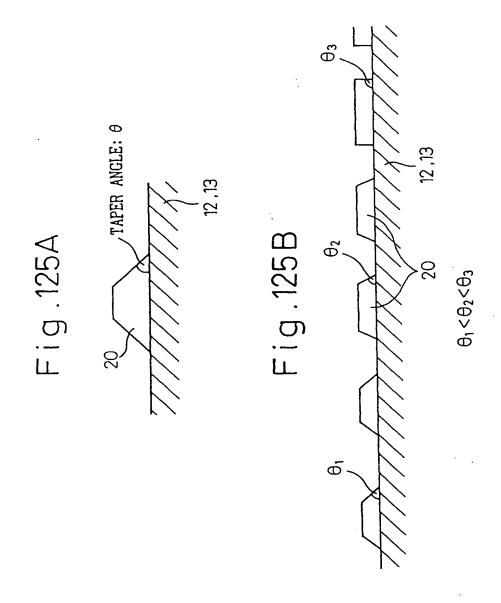


Fig.126

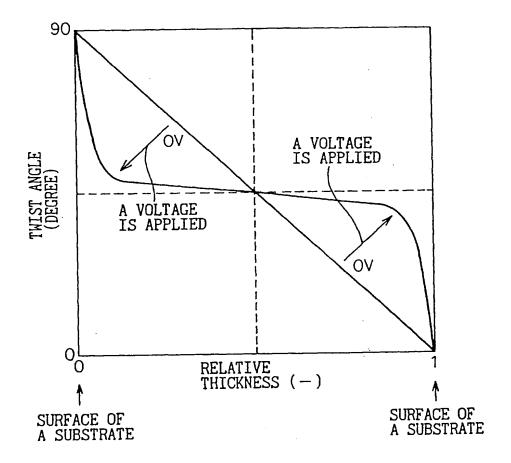


Fig. 127

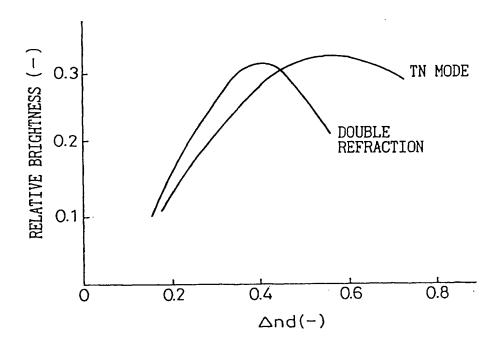


Fig.128

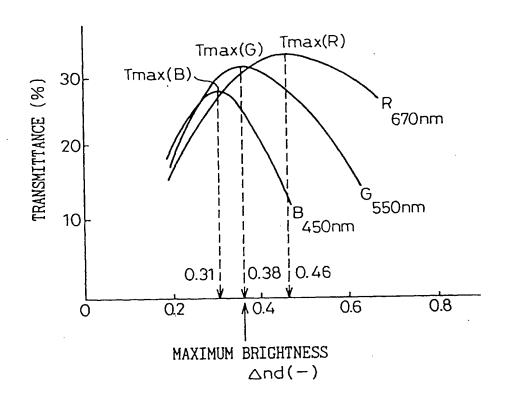


Fig.129

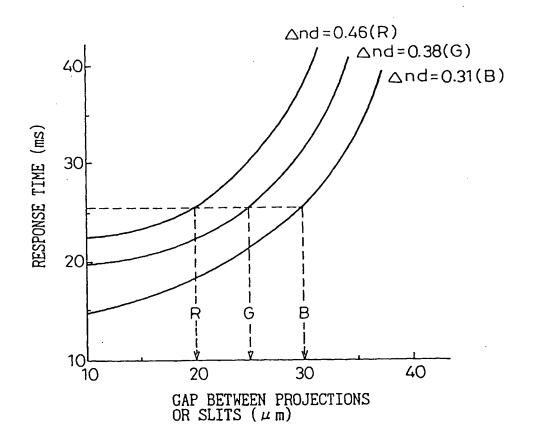
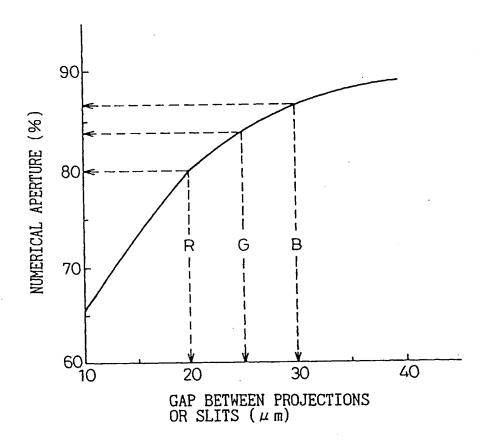
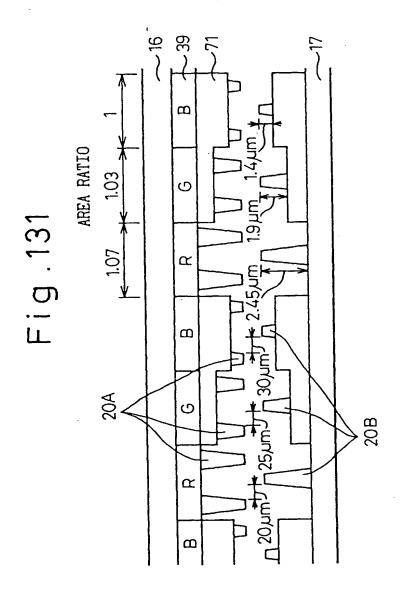


Fig.130





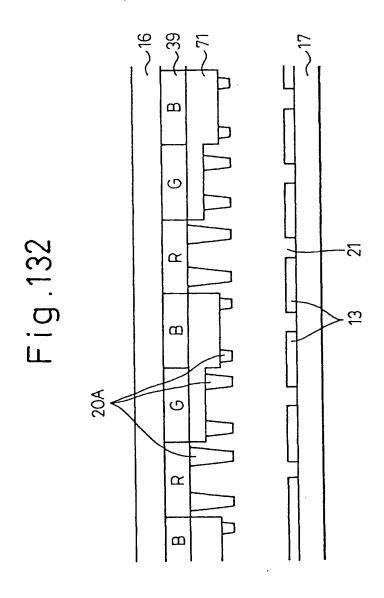


Fig.133

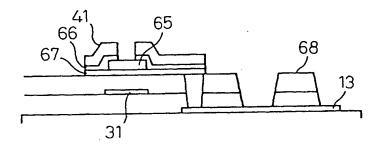
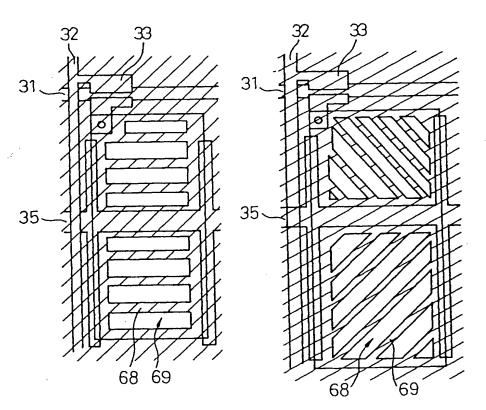


Fig.134A

Fig .134B



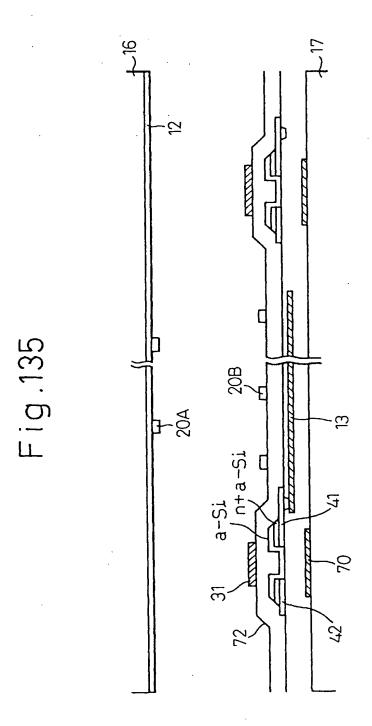
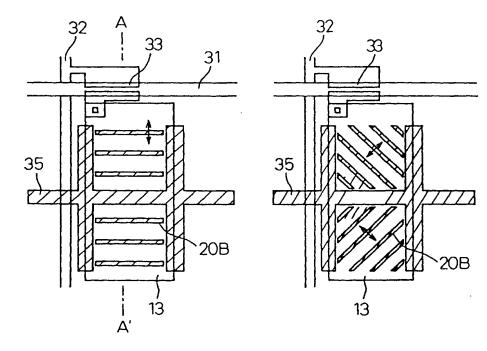
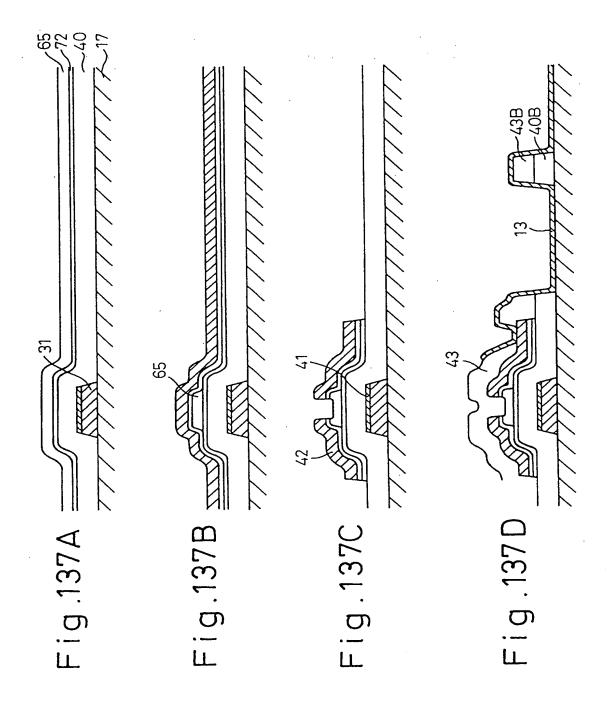


Fig.136A Fig.136B





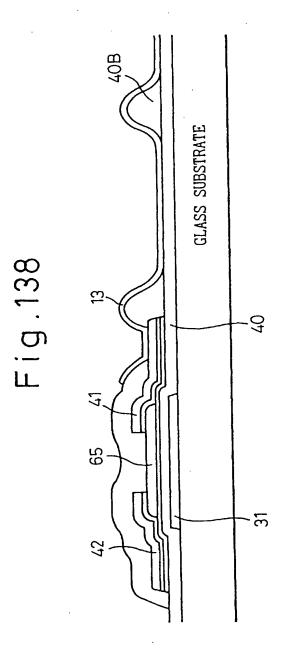
楊忠道經理,由於 920617-U1 超薄膜鋁合金高速壓鑄方法整個製作的過程,客戶所提供的資料並不完整。

故,請創字公司提供以下的事項:

- 1、 鋁合金高速壓鑄方法**詳細完整的製作流程** 例如:製作的步驟、製作過程及使用的機器。
- 2、鋁合金高速壓鑄時, **金屬溶液溫度、模具的溫 度與射出速度**在製作上參數的設定, 及配合製作過程的 情形。

從台北所 工程師 周文正 92/11/14 AM10:19

謝謝。



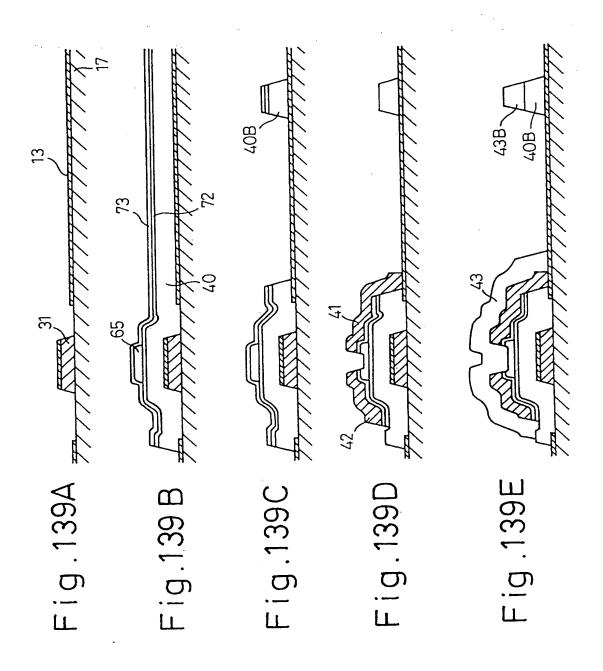


Fig.140A

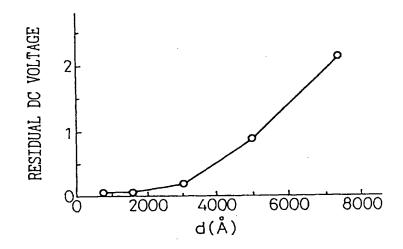


Fig.140B

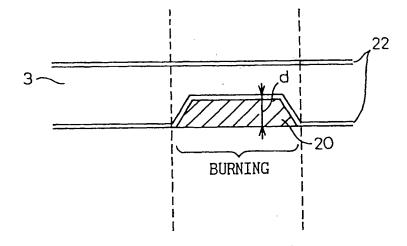


Fig.141A

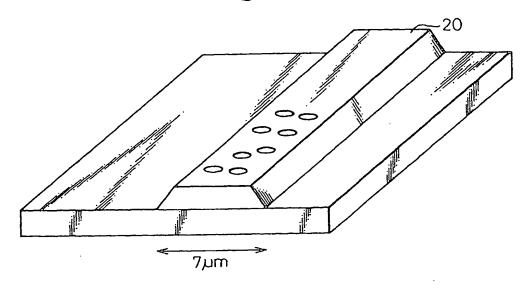
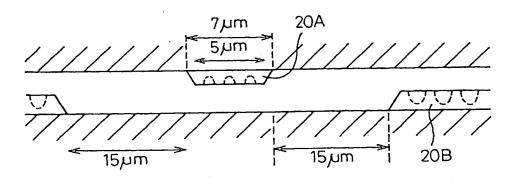


Fig.141B



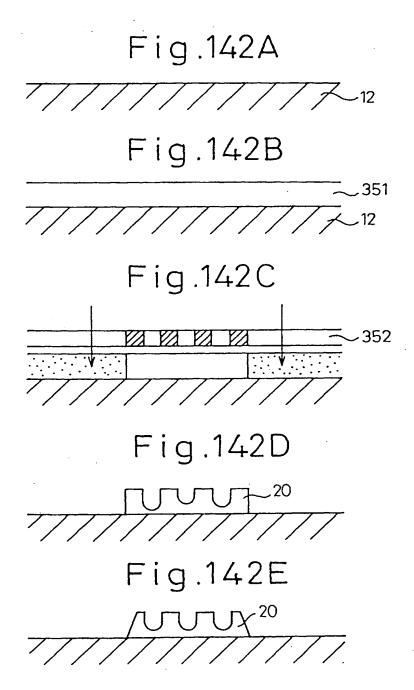
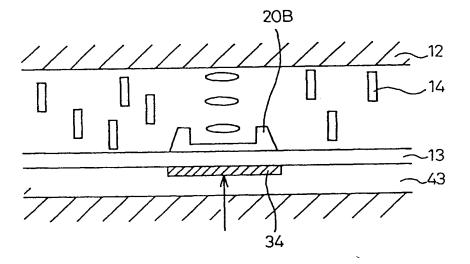
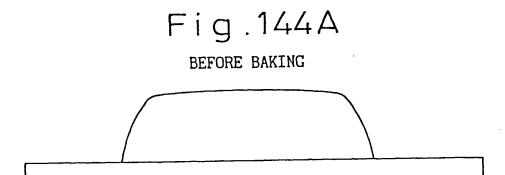
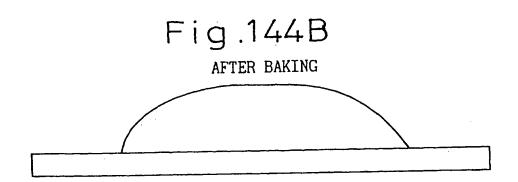
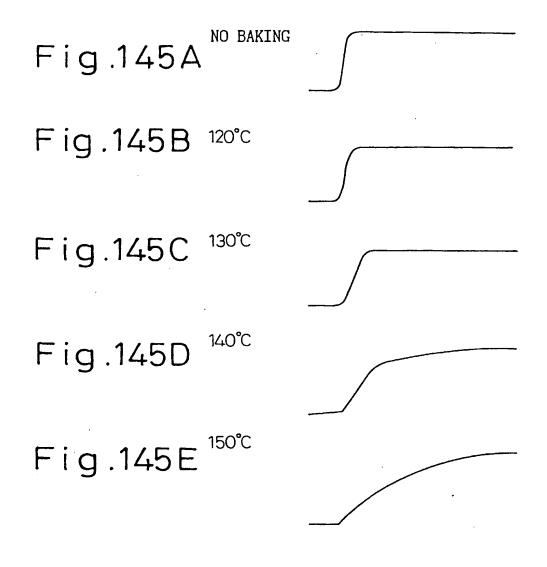


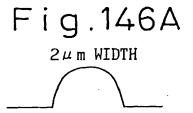
Fig.143

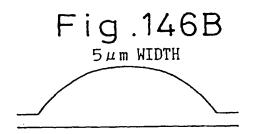












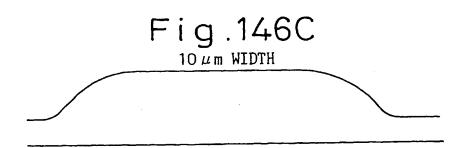


Fig.147A

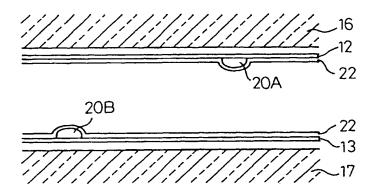
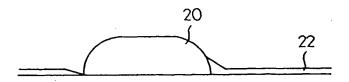


Fig.147B



## Fig.148A

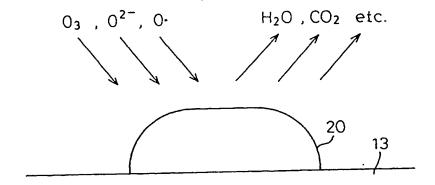


Fig.148B



Fig.148C

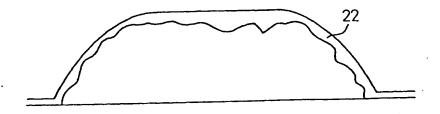


Fig.149A

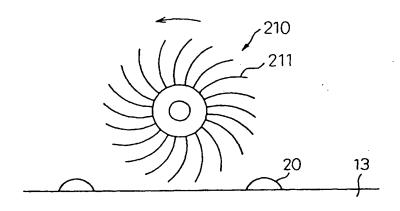
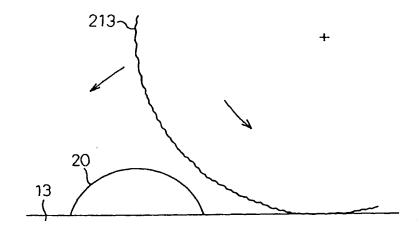
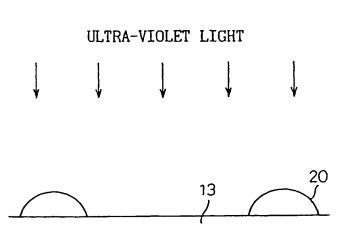
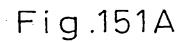


Fig.149B



## Fig.150





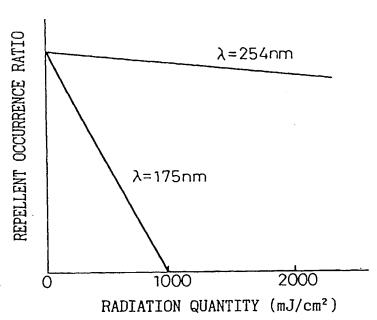
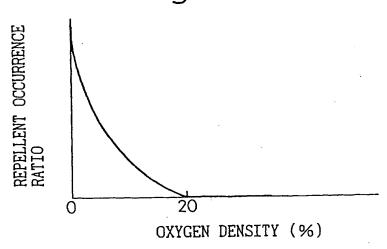
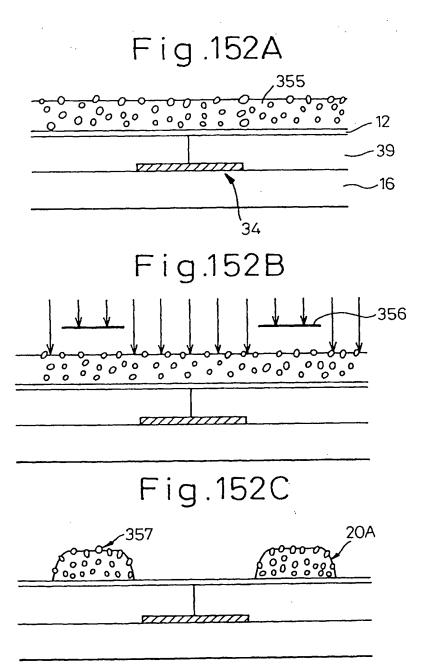


Fig.151B





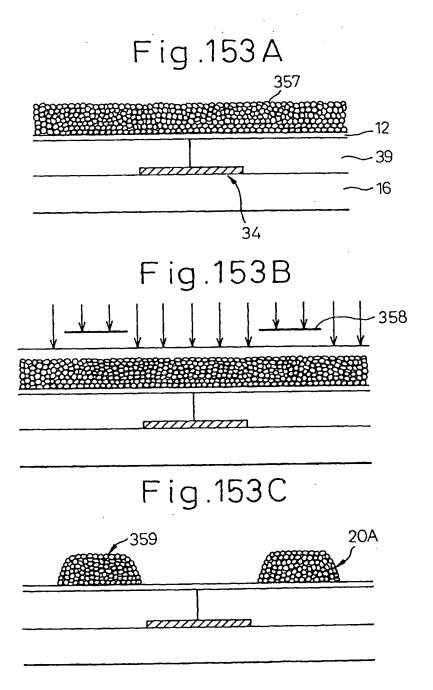


Fig.154A

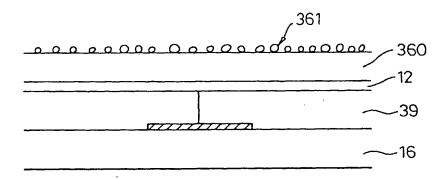


Fig.154B

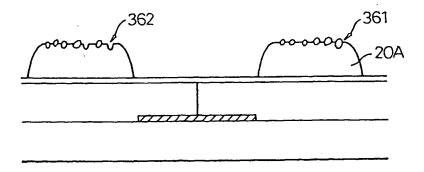


Fig.155A

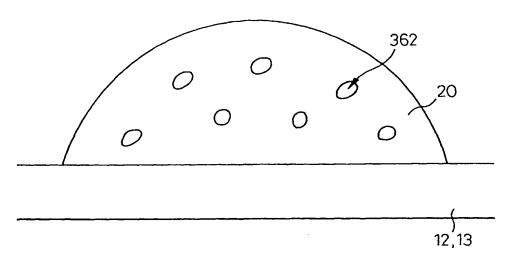
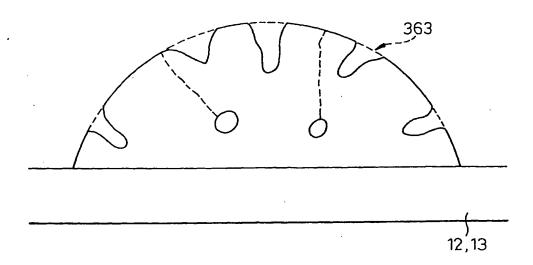


Fig.155B



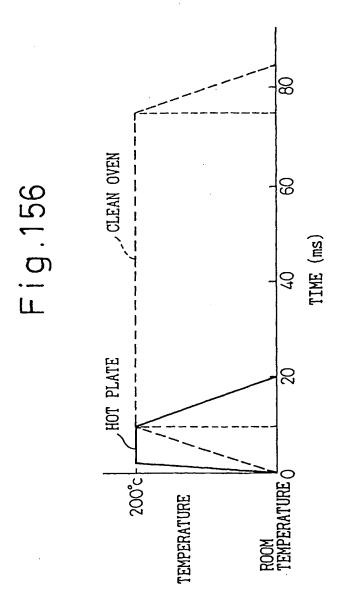


Fig.157A

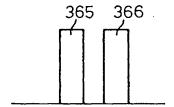


Fig.157B

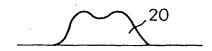
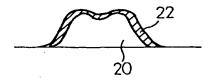
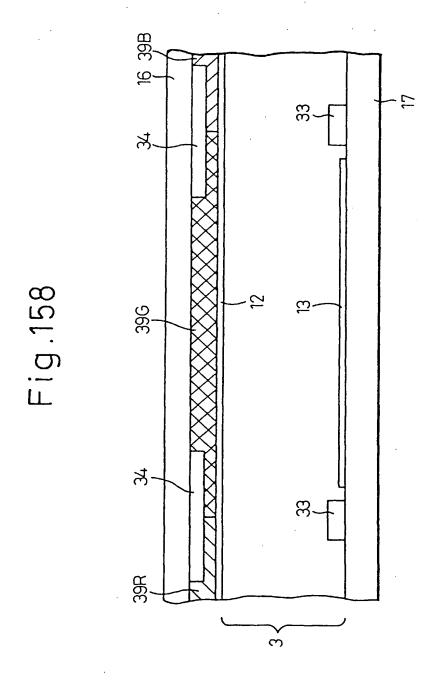


Fig.157C





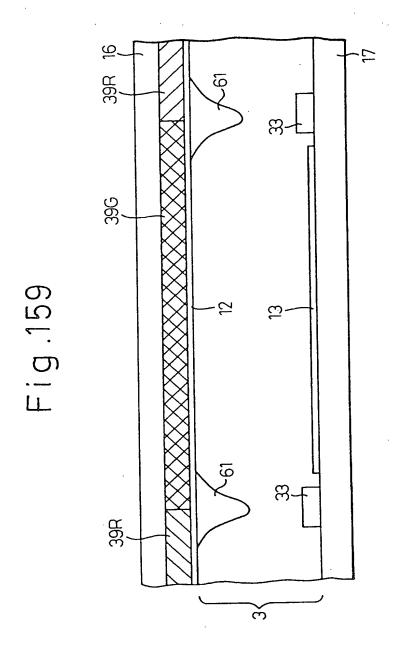


Fig.160

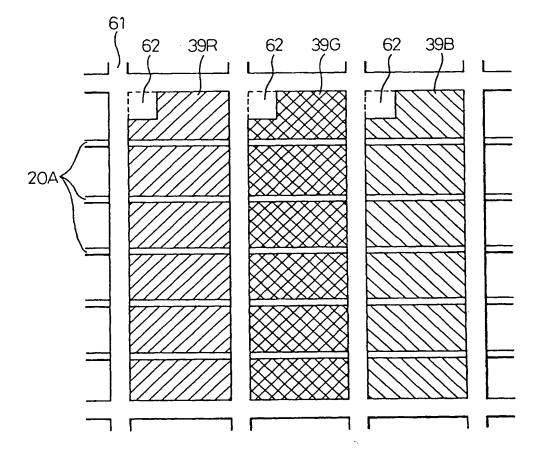
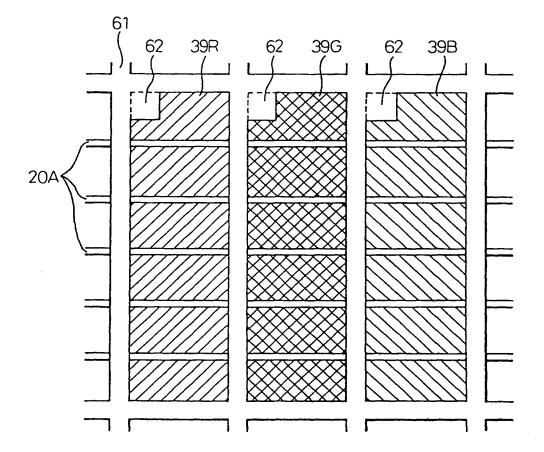
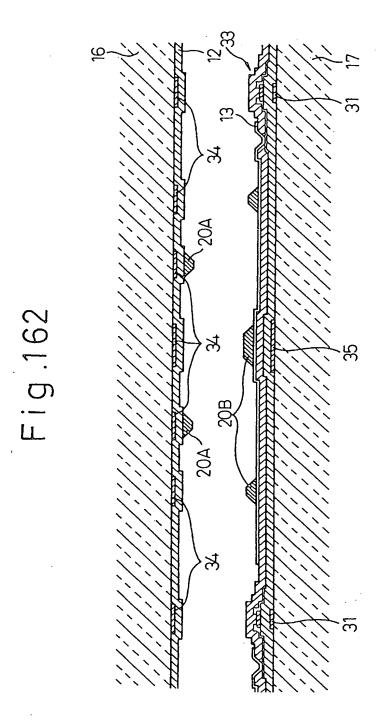


Fig.160





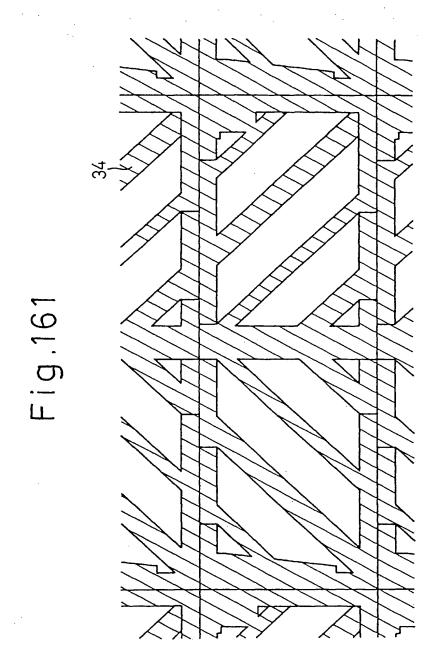
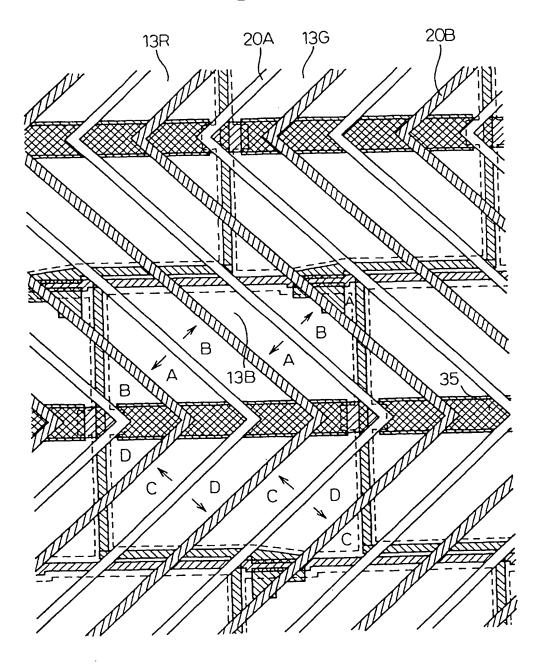
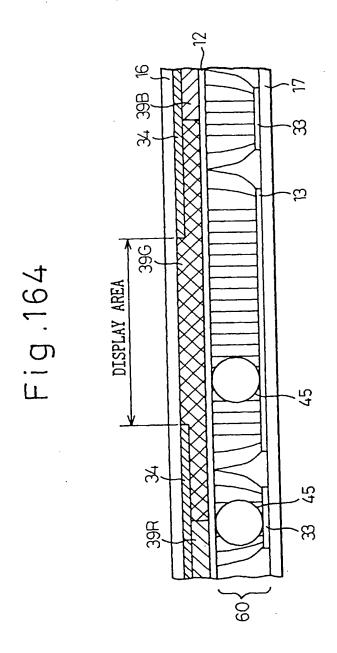
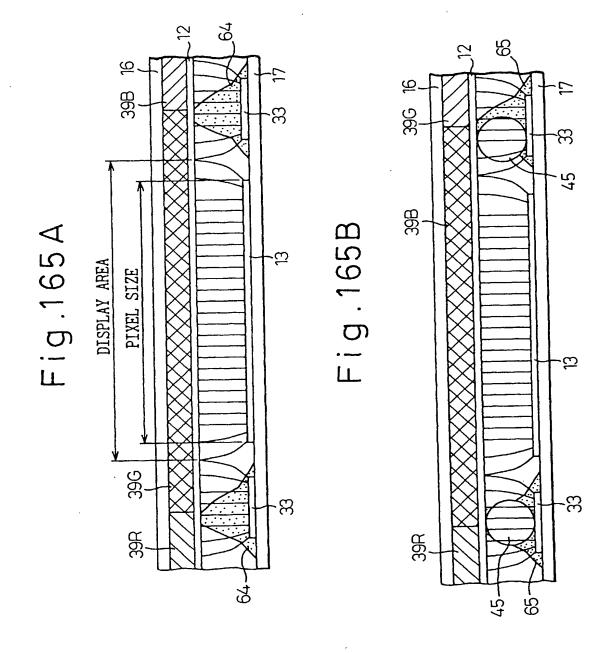
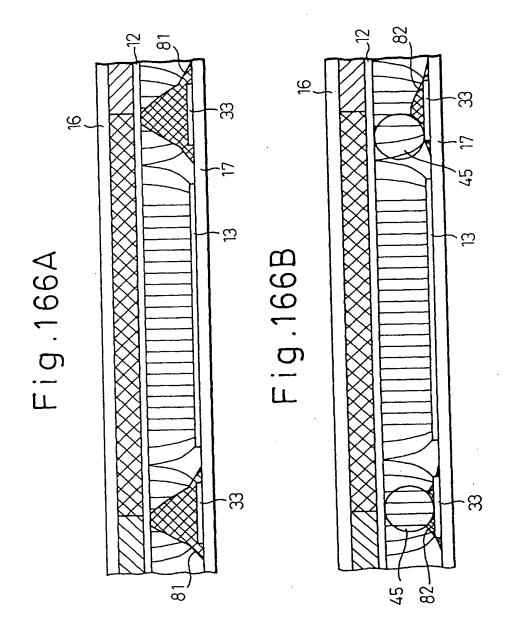


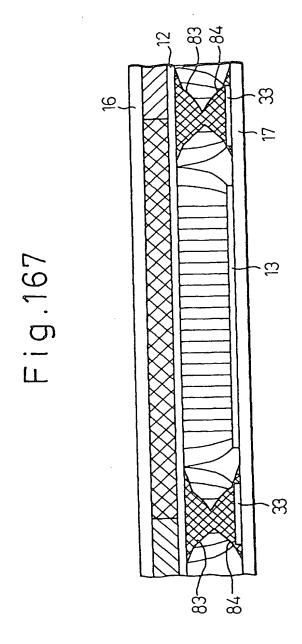
Fig.163











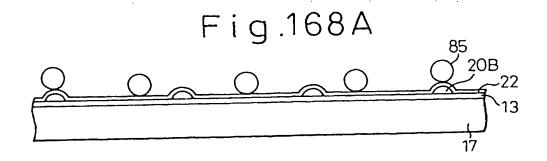
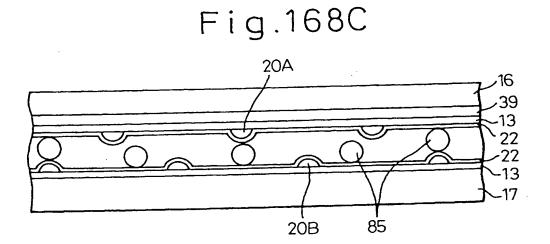
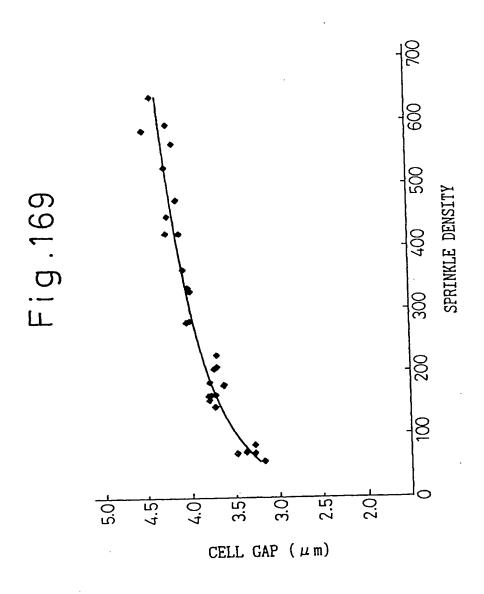


Fig.168B

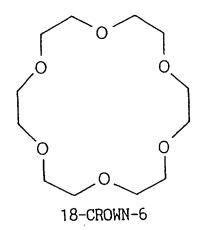




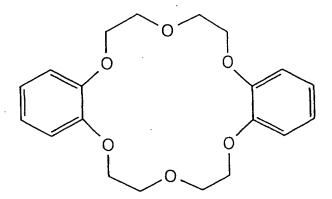
Fia.170

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(NOMBERS) IIIIII )										
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BLEMISH OCCURRENCE NO	N S	Q	SN.	Q.	윘	YES	YES	YES	YES	XEX
DOE TO POLLLING										

# Fig.171A

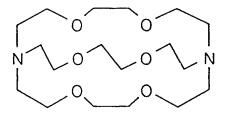


# Fig.171B



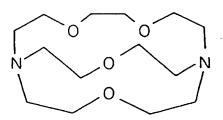
DIBENZOYL-18-CROWN-6

### Fig.172A



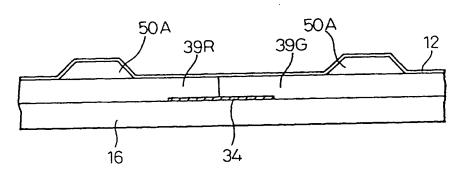
CRYPTAND [2.2.2]

### Fig.172B



CRYPTAND [2.1.1]

#### Fig.173A



#### Fig.173B

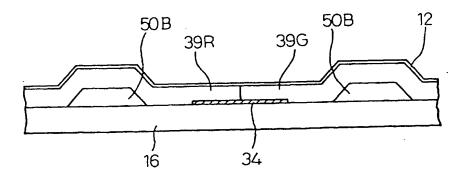


Fig.174

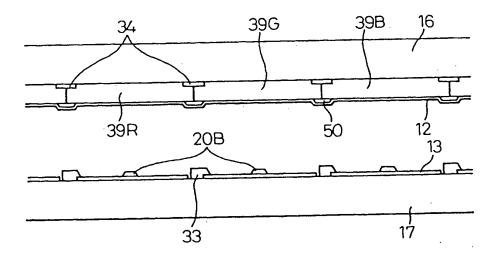


Fig.175A

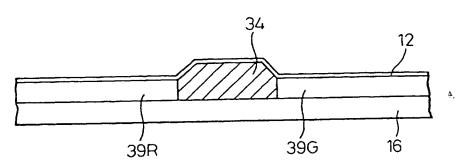


Fig.175B

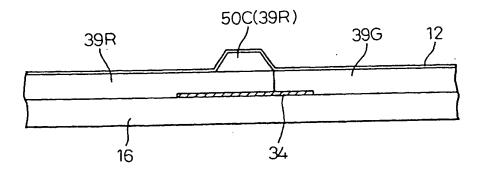


Fig.176A

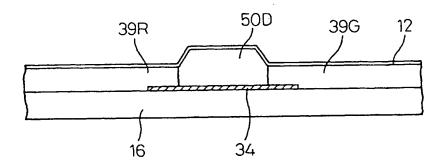


Fig.176B

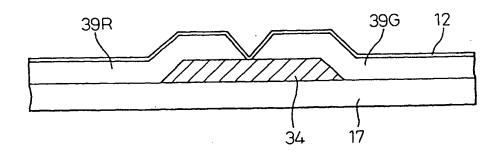


Fig.177A

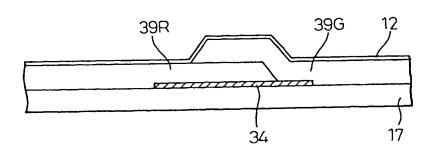
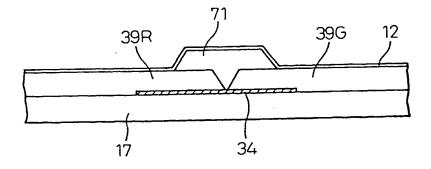


Fig.177B



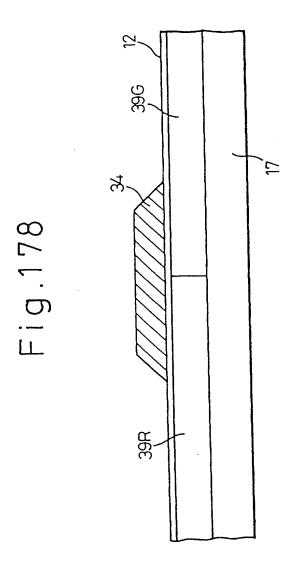


Fig.179A

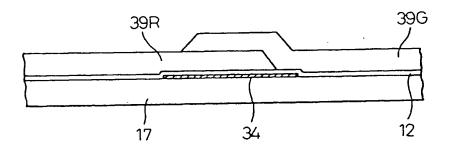


Fig.179B

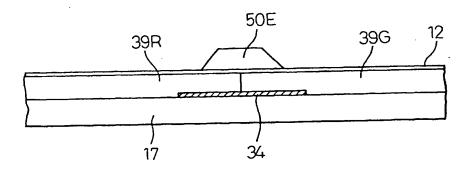


Fig.180A

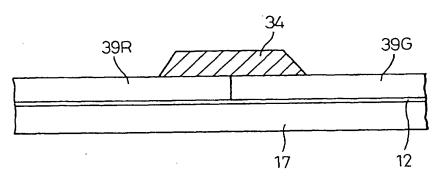
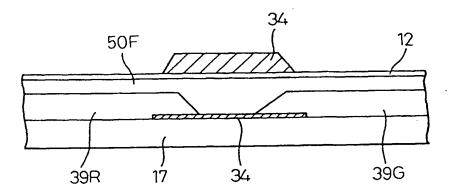
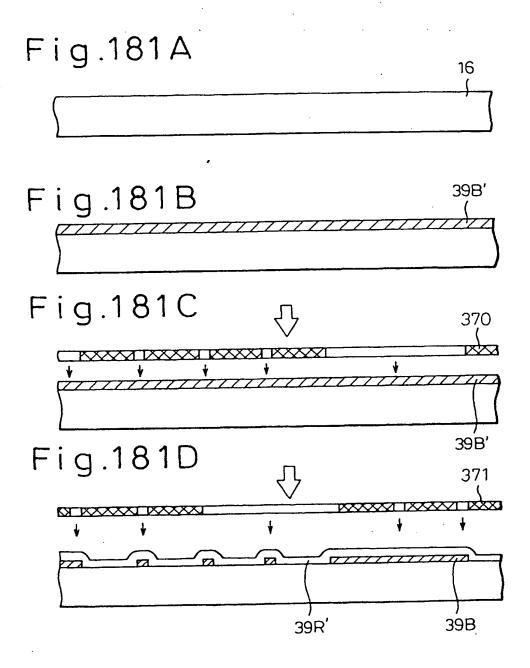


Fig.180B





## Fig.181E

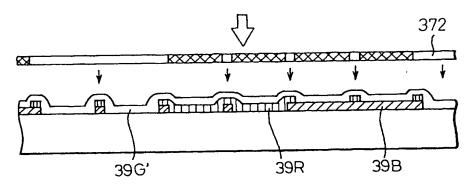


Fig.181F

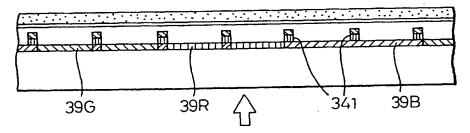


Fig.181G

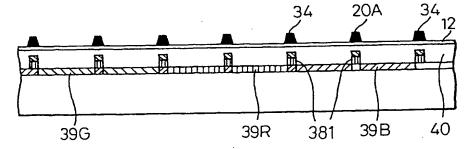
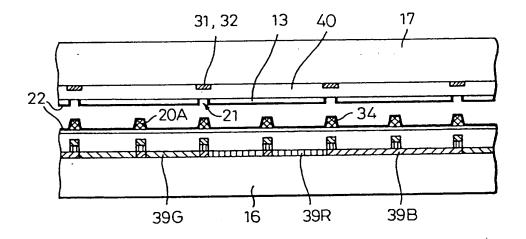
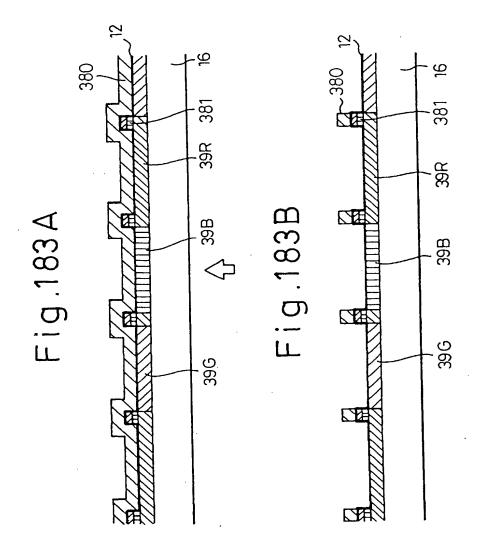
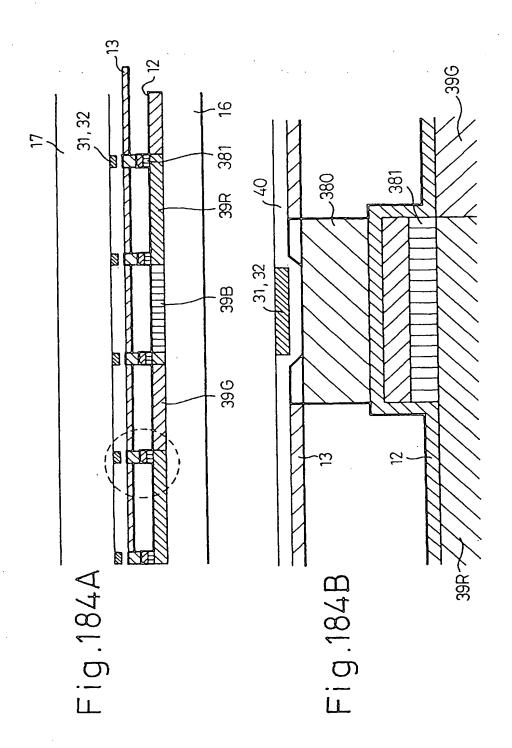
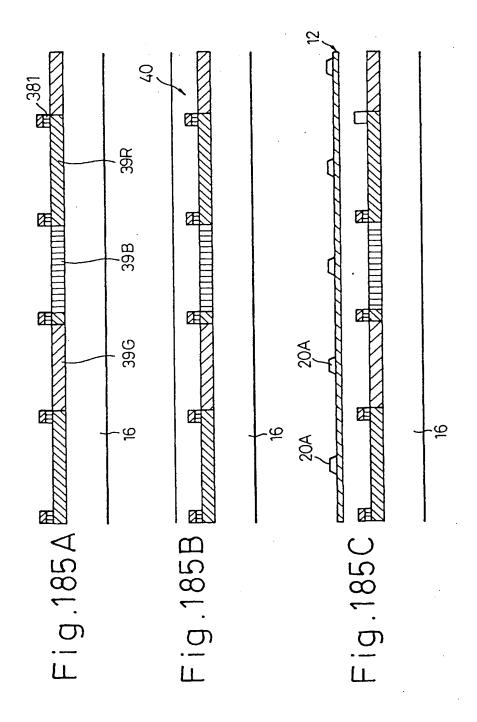


Fig.182









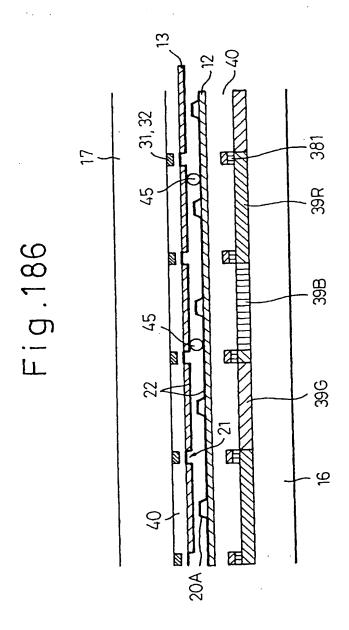
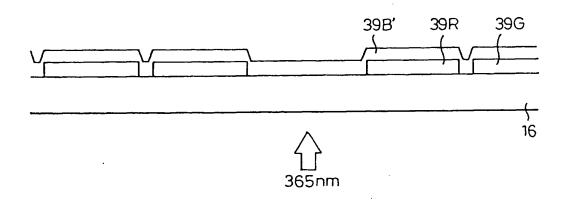


Fig.187



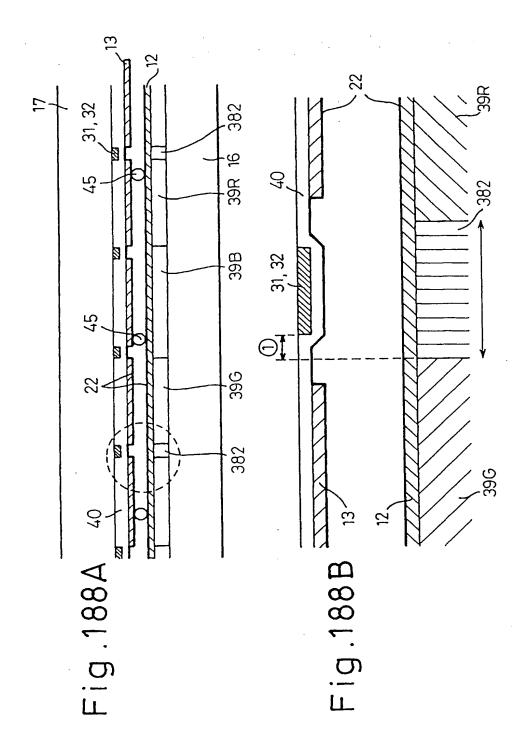
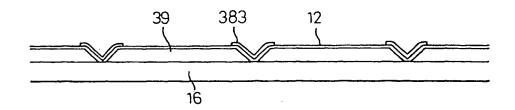


Fig.189



## Fig.190A

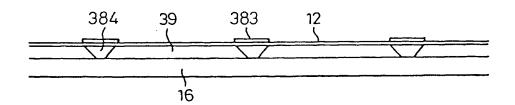


Fig.190B

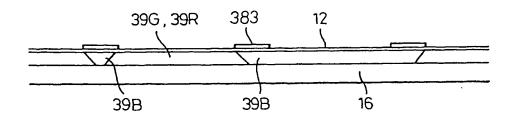


Fig.191

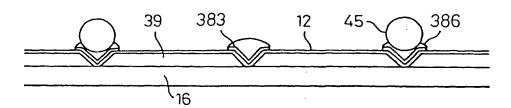


Fig.192

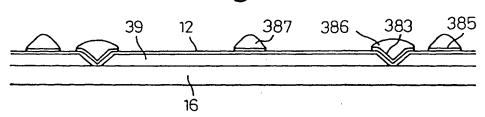


Fig.193

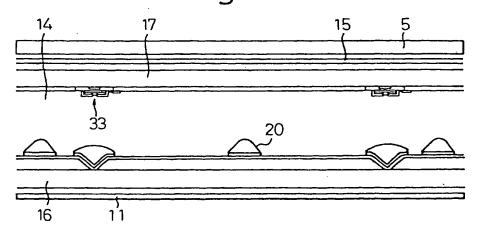


Fig.194

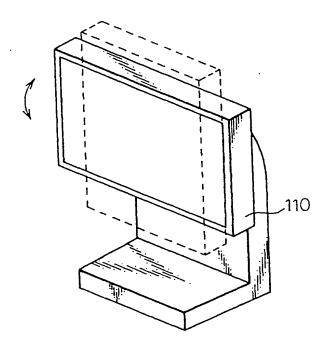


Fig.195

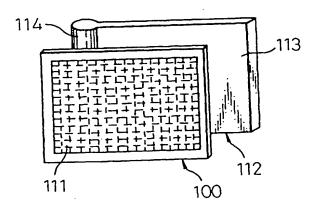
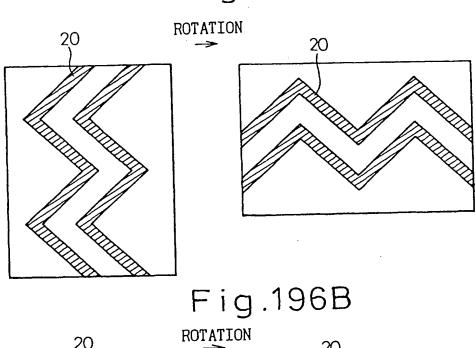


Fig.196A



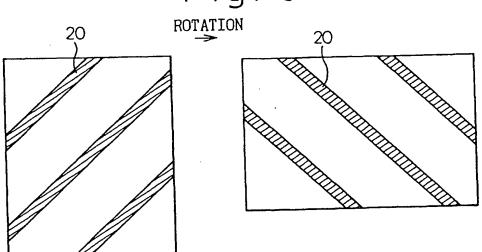


Fig.197

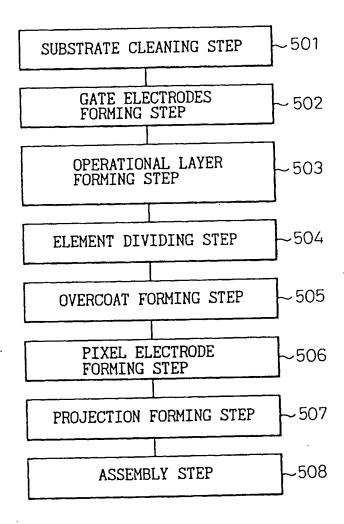


Fig.198

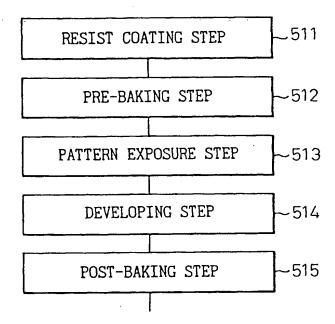
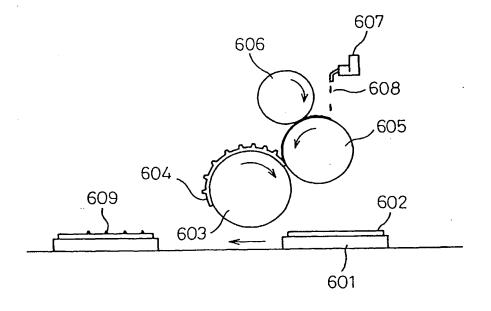


Fig.199



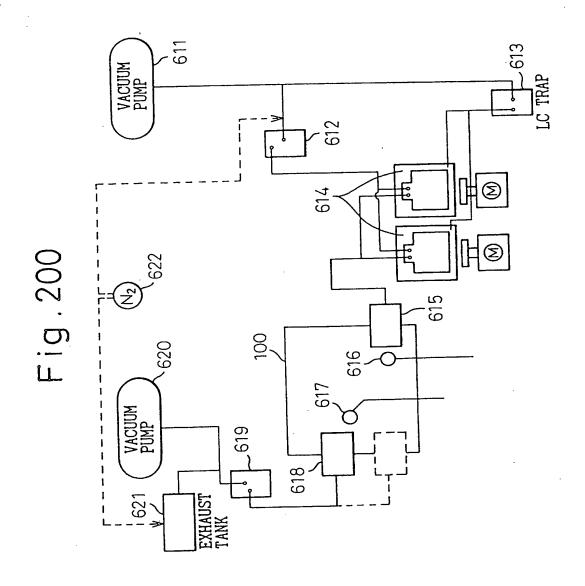


Fig. 201A

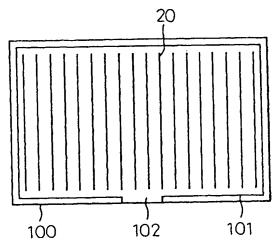


Fig.201B

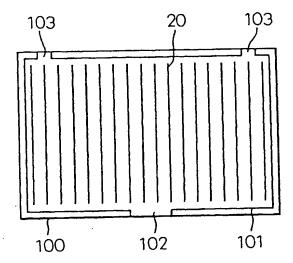


Fig.202A

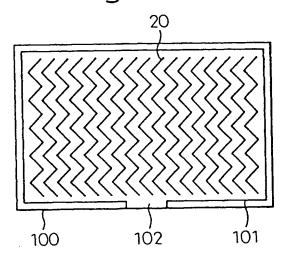


Fig. 202B

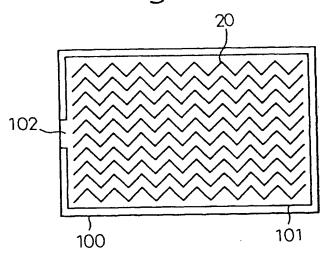


Fig. 203A

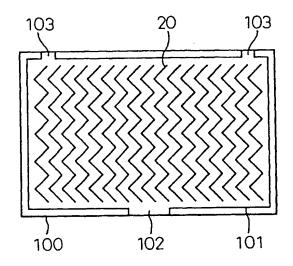


Fig.203B

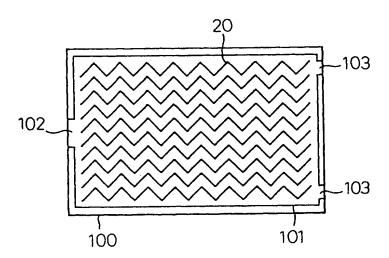


Fig. 204

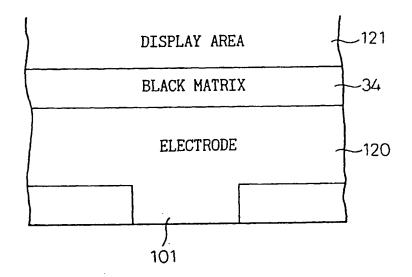


Fig.205A

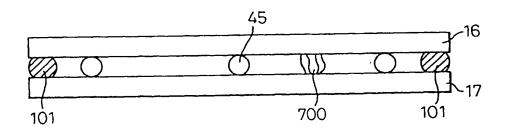


Fig.205B

700

Fig.205C

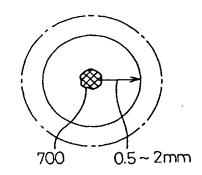
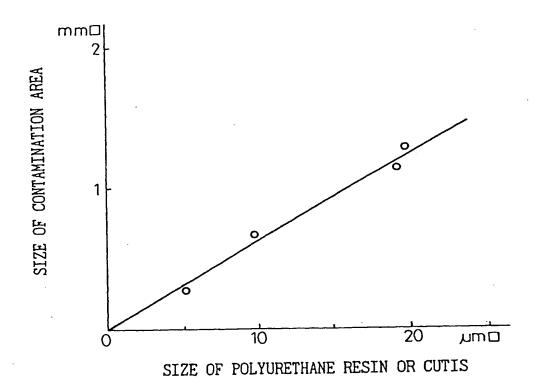
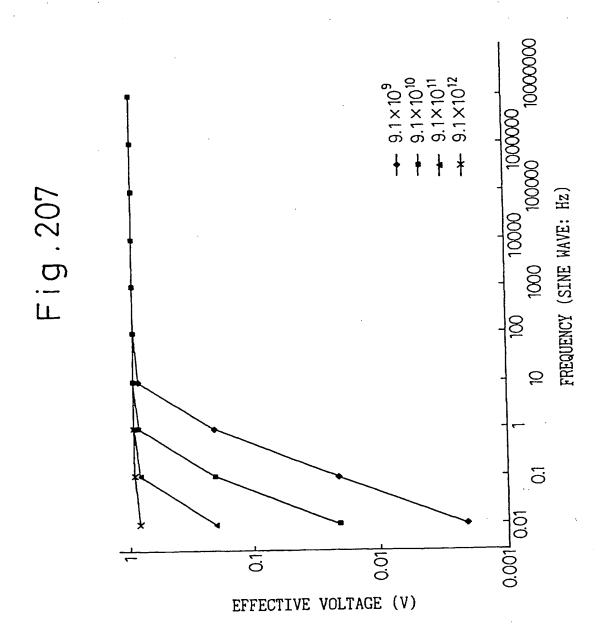
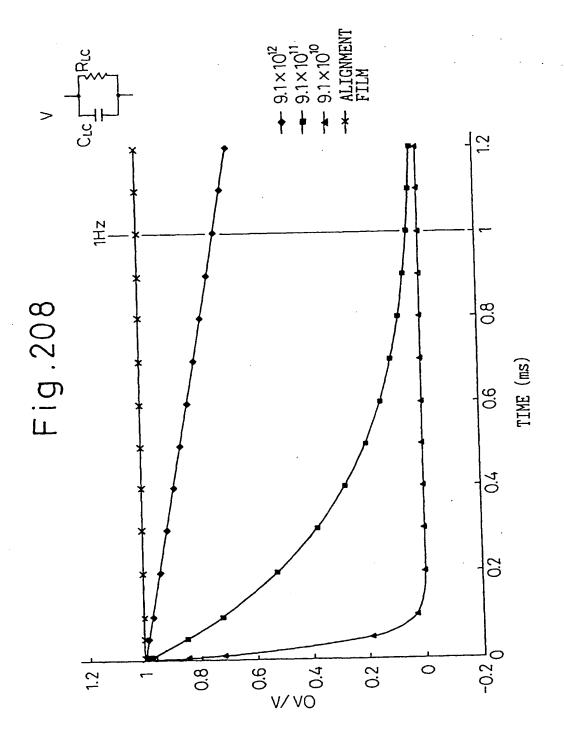


Fig.206







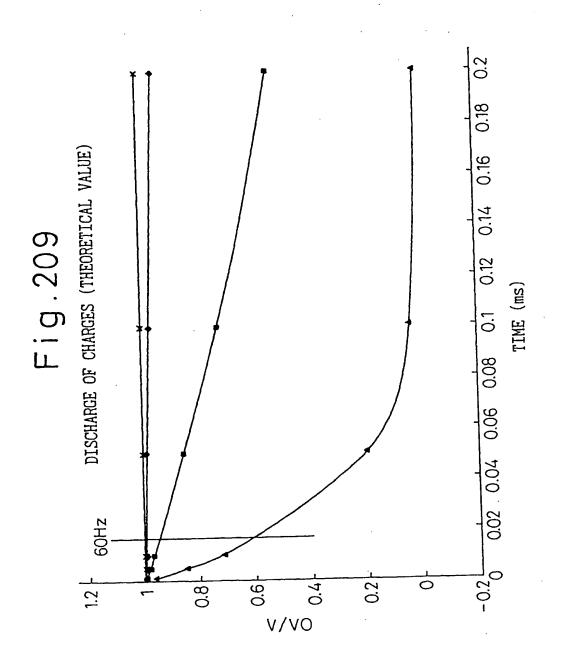


Fig.210

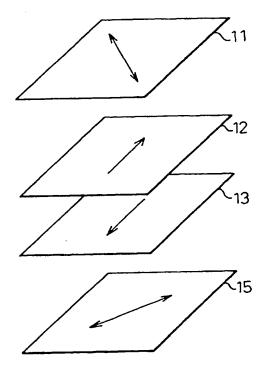


Fig. 211

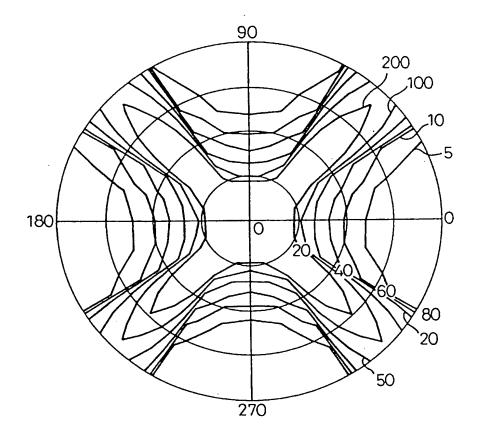


Fig.212

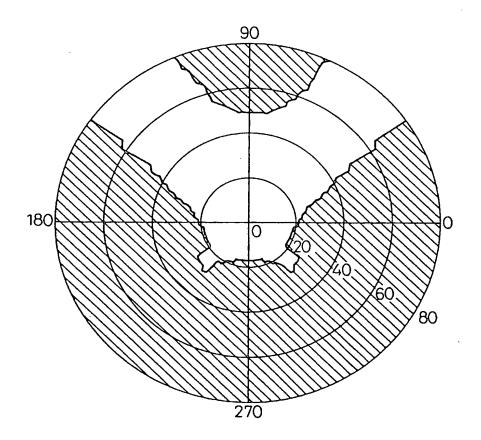


Fig.213

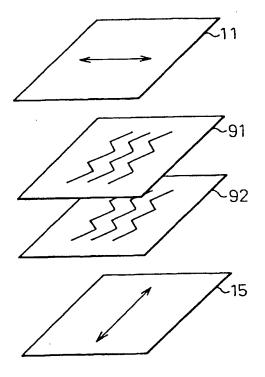


Fig. 214

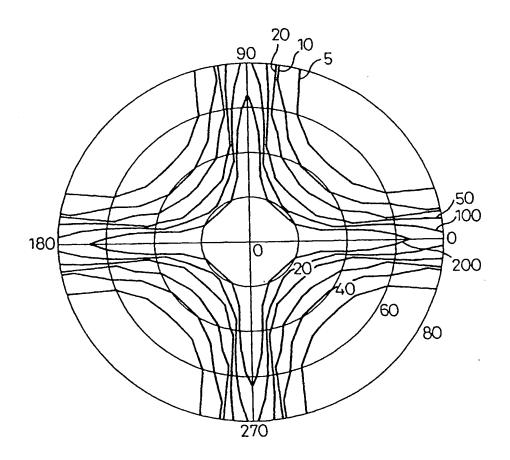
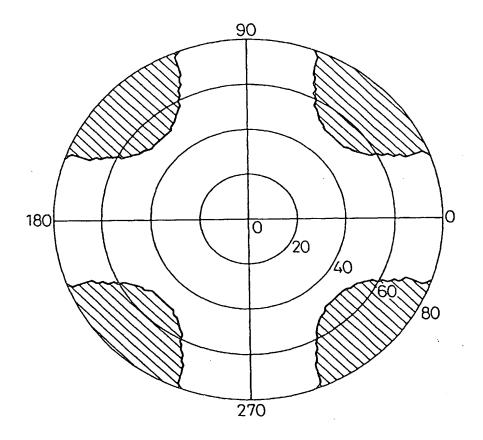
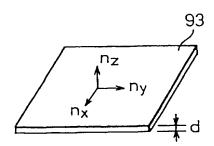


Fig.215



## Fig.216



GENERAL CONDITION

 $n_X$ ,  $n_Y \ge n_Z$ 

POSITIVE UNIAXIAL FILM

 $n_x > n_y = n_z$ 

NEGATIVE UNIAXIAL FILM

 $n_x = n_y > n_z$ 

BIAXIAL FILM (A PHASE LAG AXIS IS X DIRECTION.)

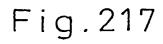
 $n_x > n_y > n_z$ 

RETARDATION IN INPLANE DIRECTIONS

 $R = (n_x - n_y)d$ 

RETARDATION OF THICKNESS DIRECTION

$$R = \left(\frac{n_x + n_y}{2} - n_z\right) d$$



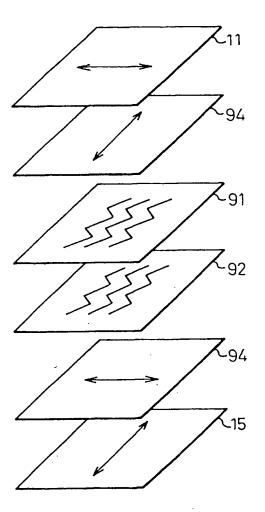


Fig.218

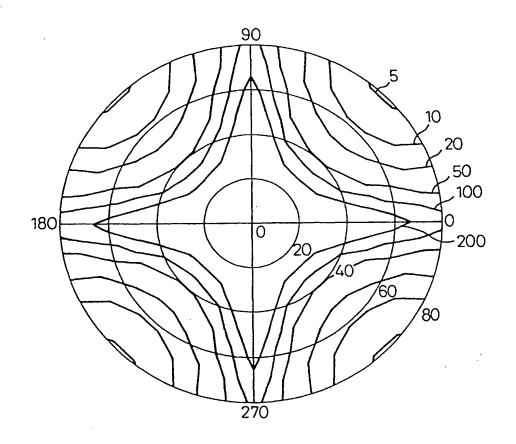
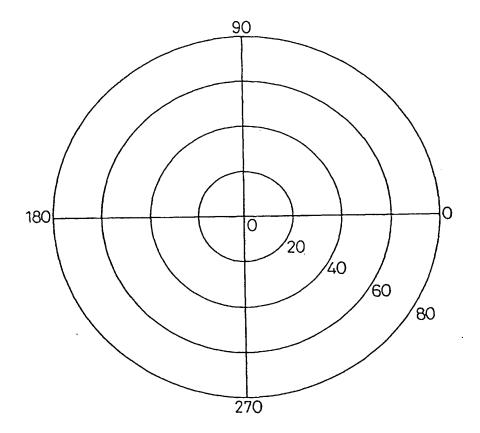


Fig.219



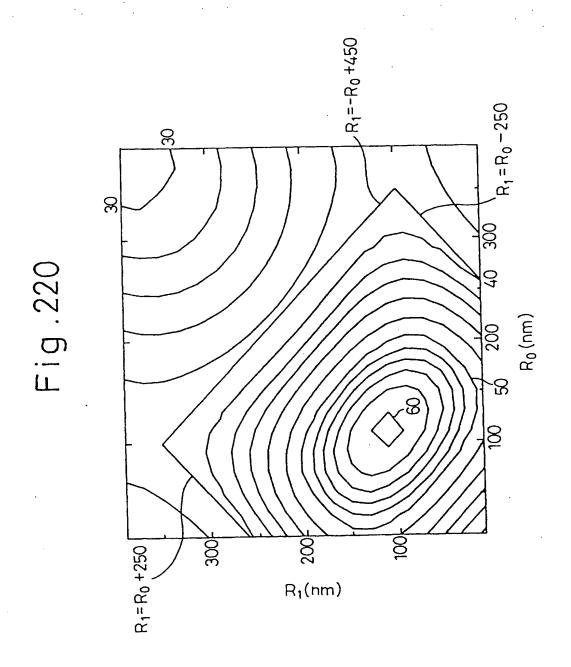


Fig. 221

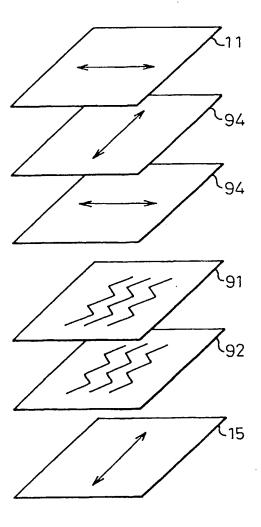


Fig. 222

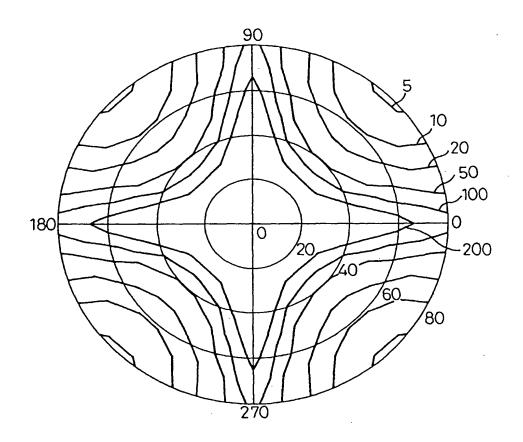


Fig.223

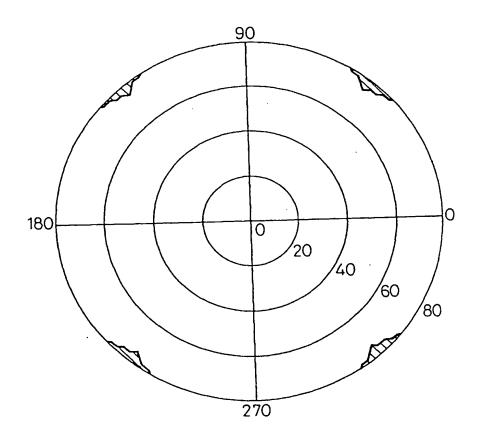


Fig.224

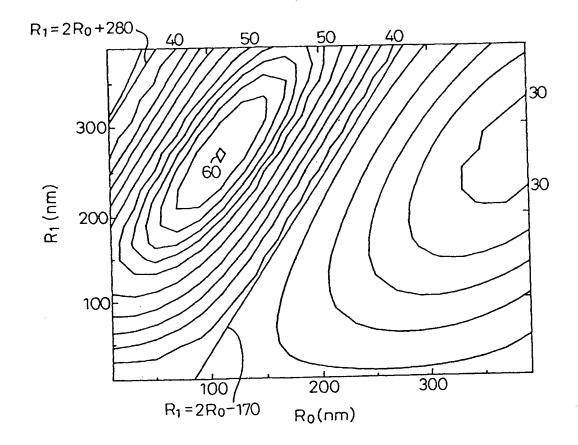


Fig.225

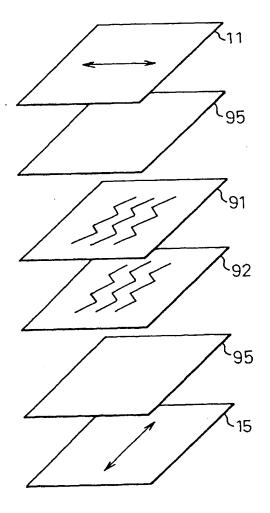


Fig.226

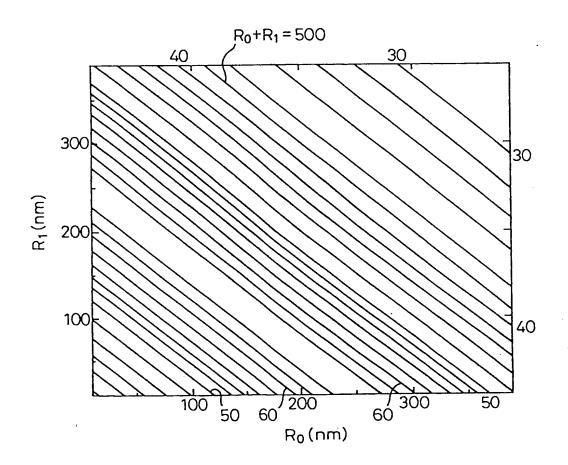


Fig.227

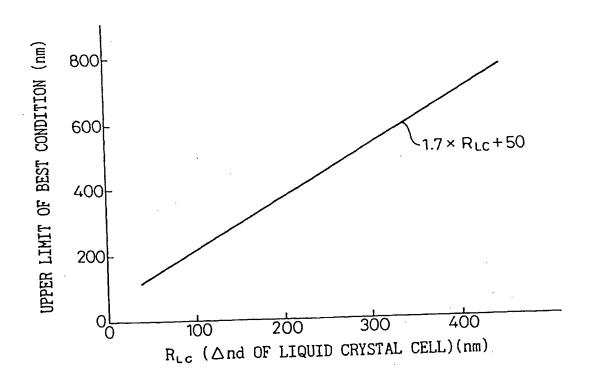


Fig.228

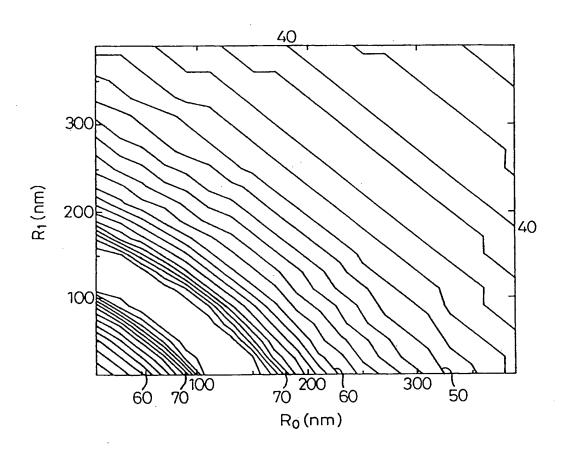


Fig.229

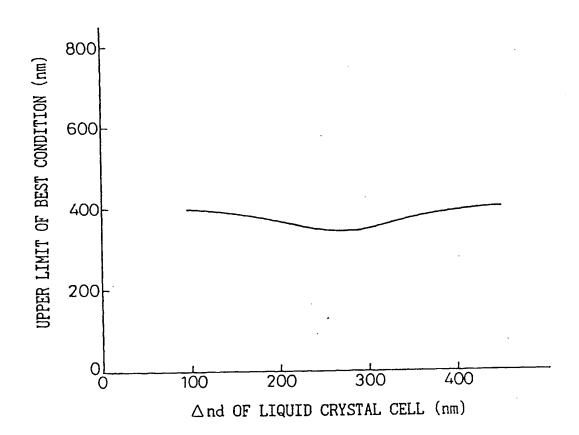


Fig.230

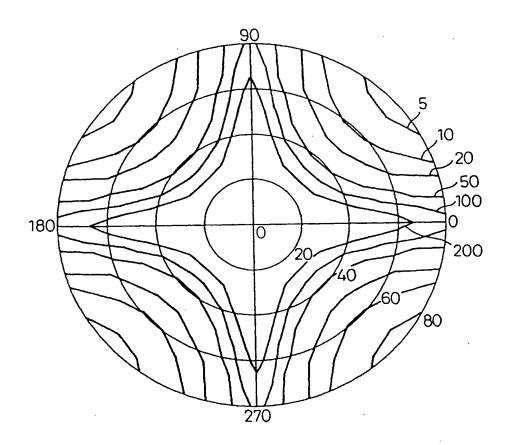


Fig. 231

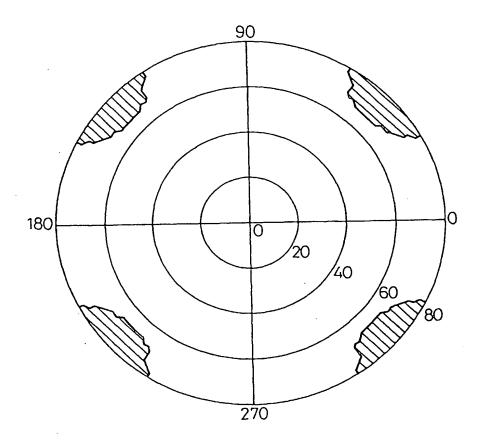


Fig.232

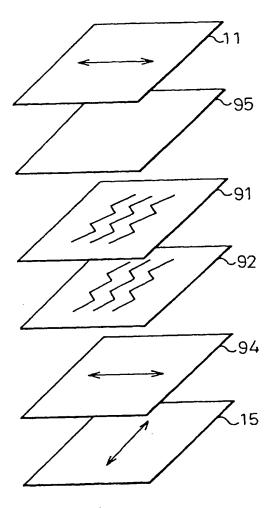


Fig.233

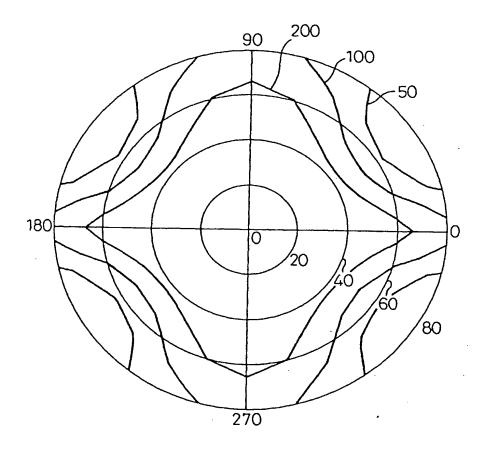


Fig. 234

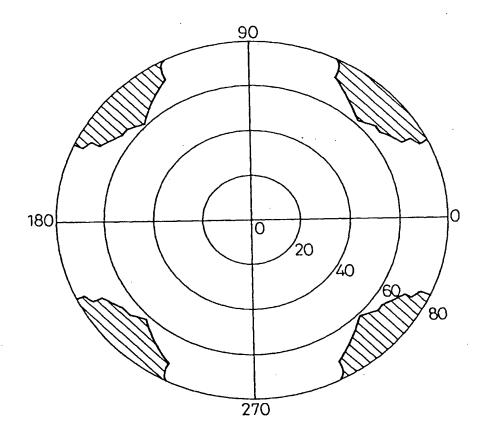


Fig. 235

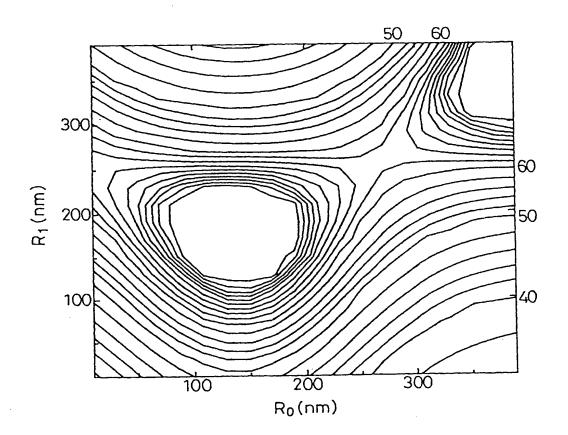


Fig.236

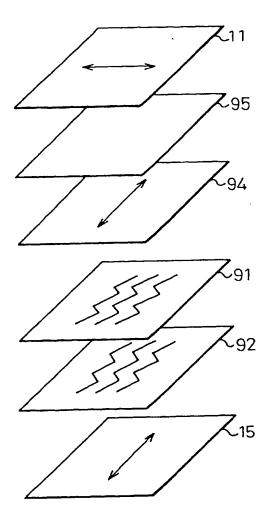


Fig.237

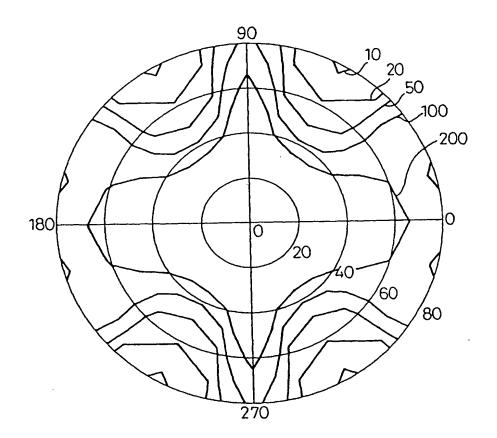


Fig.238

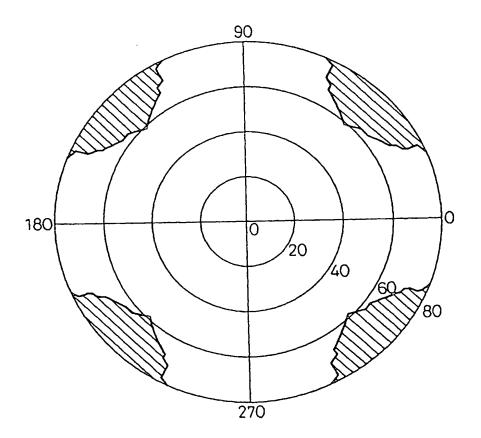


Fig.239

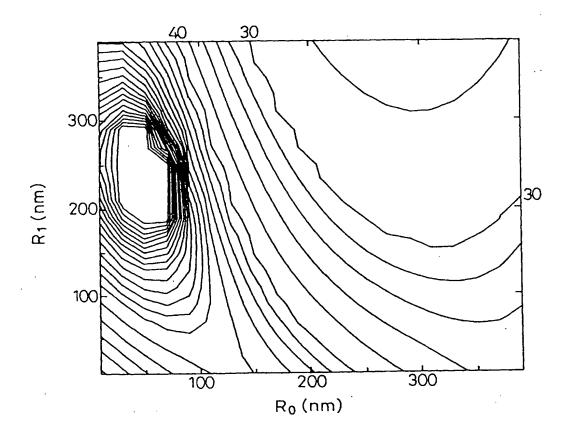


Fig. 240

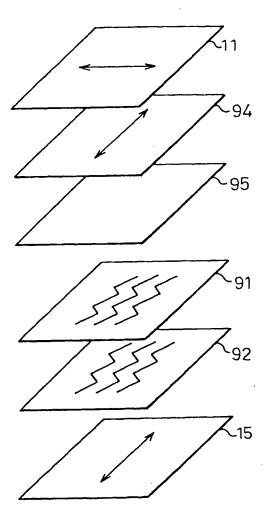


Fig.241

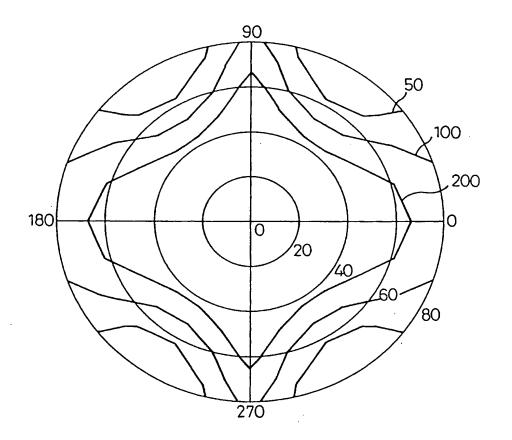


Fig. 242

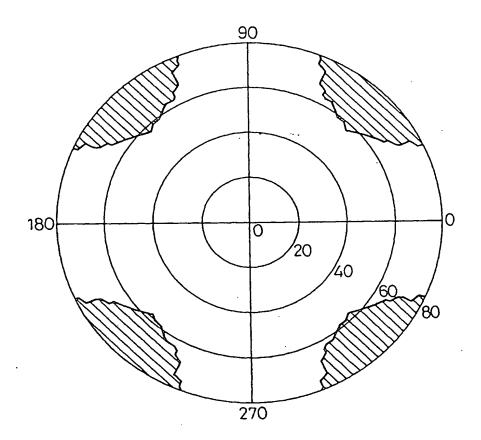


Fig.243

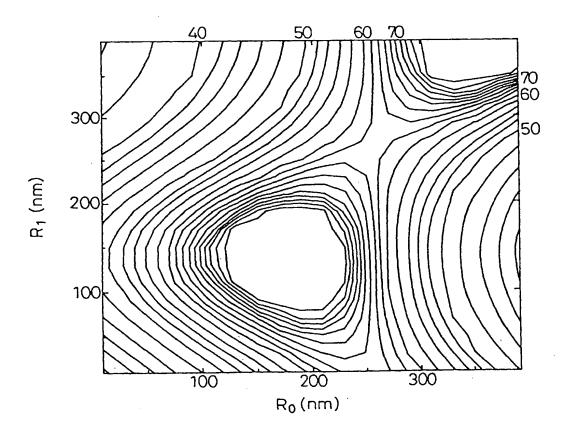


Fig. 244

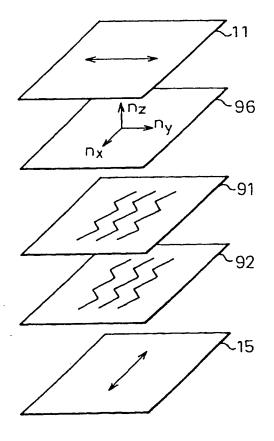


Fig.245

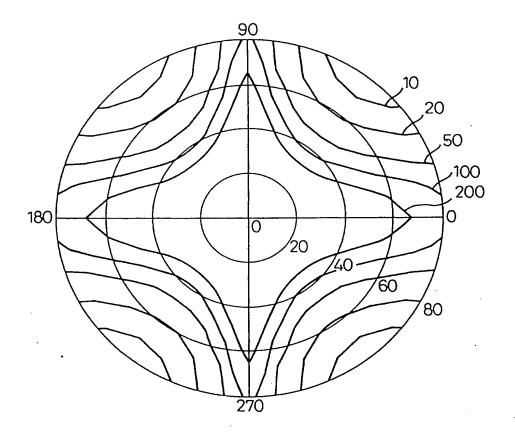
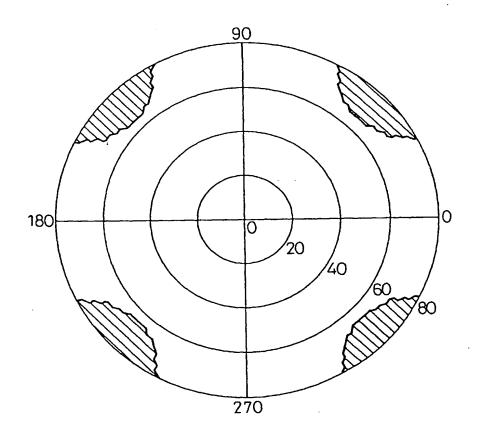


Fig. 246



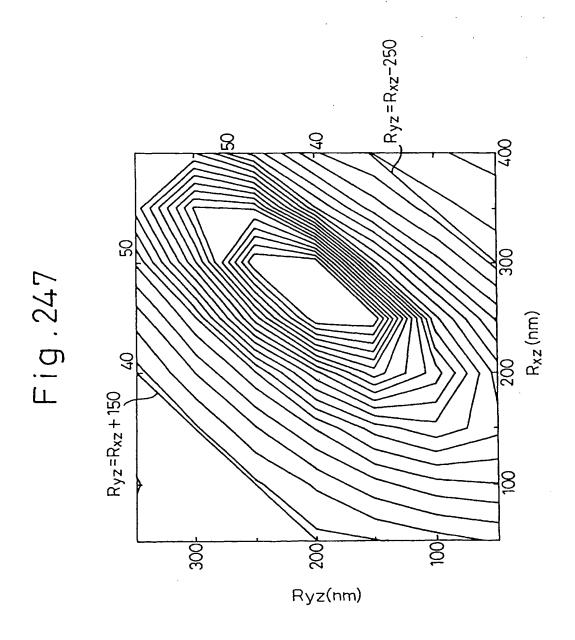


Fig.248

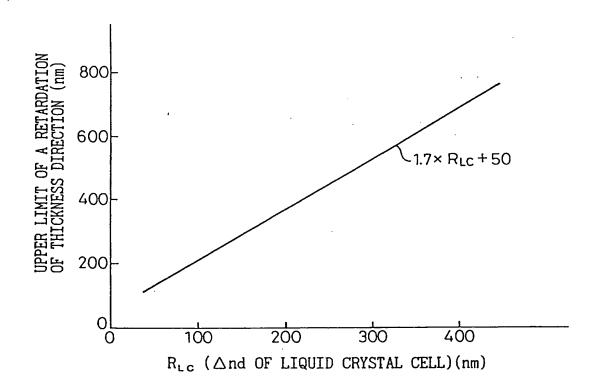


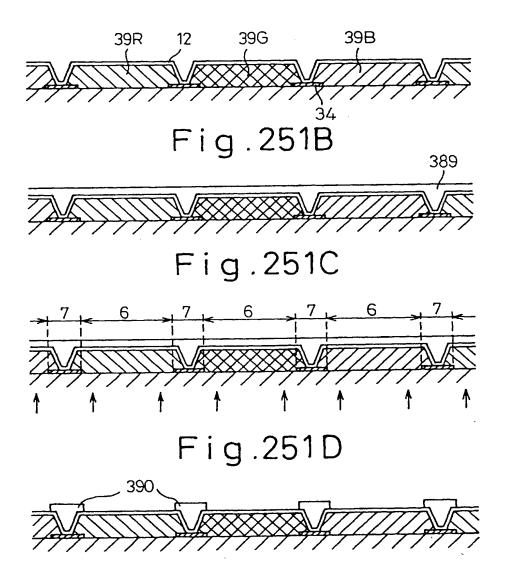
Fig. 249

SNCE	0.03	0.05	0.05	0.12
OR DIFFERENCE (5v: LEFT) -RIGHT U(x)   $\Delta v(Y)$	0	о́ 	о 	oʻ
	0.03	0.03	90.0	0.14
VIEW ANGLE: CR > 10 LEFT-RIGHT DIRECTION	± 80°	+ 80°	÷ 80°	. 80 +
TRANS- MITTANCE % (5v)	5.60	5.60	4.50	2.80
PHASE DIFFERENCE FILM Rd VALUE (nm)	320	320	240	320
GAP BETWEEN PROJECTIONS (μπ) R G B	20, 25, 30	20, 25, 30	R, G, B=30	R, G, B=30
THICKNESS OF A PANEL (µm) R G B	EMBODIMENT 5.7, 4.6, 3.6	EMBODIMENT 5.7, 4.6, 3.6	R, G, B=3.6	R,G,B=4.6
SAMPLE	EMBODIMENT	EMBODIMENT	PRIOR ART   R,G,B=	PRIOR ART R,G,B=

Fig.250

EXAMPLES	INITIAL AFTER 200 VALUES HOURS	
EMBODIMENT C	25	42
EMBODIMENT D	33	51
EMBODIMENT E	26	45
EMBODIMENT F	30	48
REFERENCE	32	70

## Fig.251A



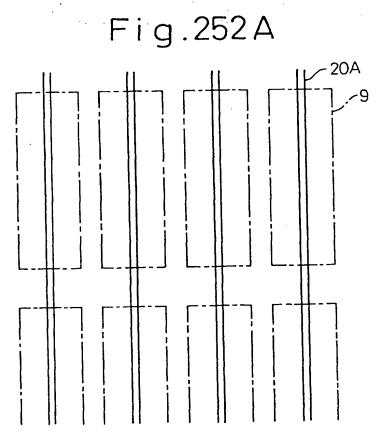


Fig.252B

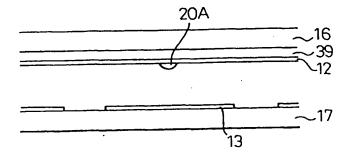
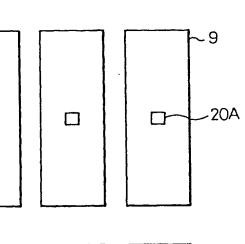
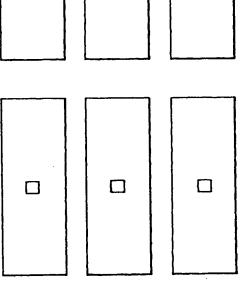


Fig. 253





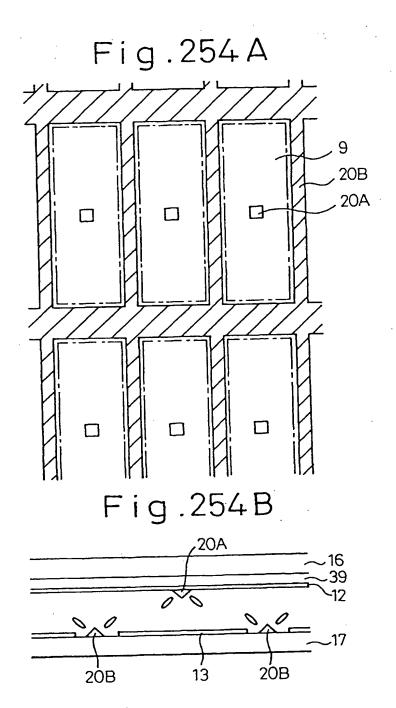


Fig.255

